## MAJOR AND MINOR LOSSES OF FLOW IN PIPES

## Major Losses

The major losses of energy are due to friction. Which are considerable hence it is called as major losses. It is determined by Darcy- Weisbach formula and Chezy's formula. Head loss due to friction is denoted by $\mathrm{h}_{\mathrm{f}}$.

## Darcy- Weisbach formula

$$
\mathrm{h}_{\mathrm{f}}=\frac{4 \mathrm{fL} V^{2}}{2 g d}
$$

Where, hf - loss of head due to friction in meter of fluid
f - Coefficient of friction
Coefficient of friction is function of Reynolds's Number (Re).
If $R e$ is less than 2000 (i.e. laminar flow) $f=\frac{16}{R e}$
If Re is greater than 4000 (i.e. turbulent flow) $\mathrm{f}=\frac{0.0719}{R e^{1 / 4}}$
L- Length of pipe in $m$.
V- Velocity of flow in $\mathrm{m} / \mathrm{s}$.
$d$ - Diameter of pipe in $m$.
Let, $\mathrm{V}=\frac{Q}{A}$, Hence Darcy-Weisbach formula in the term of discharge Q ,

$$
\mathrm{h}_{\mathrm{f}}=\frac{\mathrm{fL} Q^{2}}{12 d^{5}}
$$

## Chezy's formula-

$$
V=C \sqrt{m i}
$$

Where V - velocity of flow in $\mathrm{m} / \mathrm{s}$
C - Chezy's constant
i - Loss of head per unit length of pipe $=\frac{h f}{L}$
$\mathrm{m}-$ Hydraulic mean depth $=($ Area of flow $/$ Perimeter $)=\mathrm{A} / \mathrm{P}$
$\mathrm{m}=\frac{d}{4}$ for pipe flow

## Minor losses

The losses due to disturbances in flow pattern or due to change in velocity are called as minor losses. These losses may occur due to sudden change in the area of flow and the direction of flow. These losses are less as compare to major losses. The minor loss of the head (energy) includes the following cases:

1. Loss of head due to sudden enlargement
2. Loss of head due to sudden contraction
3. Loss of head at the entrance of a pipe
4. Loss of head at the exit of a pipe
5. Loss of head due to bends
6. Loss of head in various pipe fittings
7. Loss of head due to obstruction

## 1. Loss of head due to sudden enlargement

Fig. represents a pipe in which fluid experiences sudden enlargement. Here the head lossoccurs due to the separation of the flow at the periphery of the smaller pipe, which leads to eddying motion in the corner region.


The Equation gives head loss due to sudden expansion.

$$
h e=\frac{\left(V_{1}-V_{2}\right)^{2}}{2 g}
$$

Where, V1 = Velocity of fluid at section 1-1
$\mathrm{V} 2=$ Velocity of fluid at section 2-2

## 2. Loss of Head Due to Sudden Contraction

Fig. represents a pipe in which fluid experiences sudden contraction. The stream lines are converging from section 11 to section C-C. The head loss occurs only after the vena contracta CC. This is because the flow up to this section is accelerating and the boundary
 layer separation does not occur.

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Using Bernoulli's equation, continuity and momentum equation at section 1-1 and 2-2, it can be proved that head loss due to sudden contraction is,

$$
\mathrm{hc}=\left(\frac{1}{c_{c}}-1\right)^{2} \frac{v_{2}^{2}}{2 g}
$$

Where, V2 = Velocity of fluid at section 2-2
$\mathrm{Cc}=$ Coefficient of contraction $=\mathrm{Ac} / \mathrm{A} 2$
If Cc not given,

$$
\mathrm{hc}=0.5 \frac{v_{2}^{2}}{2 g}
$$

## 3. Loss of Head at the entrance of a pipe

The loss of head at the entrance of pipe is a similar case to loss of head due to sudden contraction as there is an abrupt reduction in area from an area of reservoir to area of a pipe. The loss of head is caused mainly by the turbulence created by the sudden enlargement of the jet after it has passed through the vena contracta.

$$
\mathrm{h}=0.5 \frac{v^{2}}{2 g}
$$

## 4. Loss of head at the exit of a pipe

When the fluid from the pipe enters into a relatively larger reservoir the entire velocity is dissipated. If V is the velocity of fluid in a pipe, the head loss at exit is given by

$$
\mathrm{h}=\frac{v^{2}}{2 g}
$$

## 5. Loss of head due to bends

The loss of head in bends provided in pipes may be expressed as,

$$
\mathrm{h}=\mathrm{k} \frac{v^{2}}{2 g}
$$

V is the mean velocity of flow of liquid and $\mathrm{K}=$ coefficient of bend and is depends on the angle of bend, radius of the curvature and diameter of pipe.

## 6. Loss of Head in Various Pipe Fittings

Pipe fittings in a piping system cause obstruction to flow and the loss of head occurs. The loss of head may be expressed as,

$$
\mathrm{h}=\mathrm{k} \frac{v^{2}}{2 g}
$$

Where, $\mathrm{K}=$ Coefficient of pipe fitting
Various pipe fitting shown in following figure,

(a) Bend

(c) V Junction

(b) Tee junction

(d) Partially closed valvo

## 7. Loss of head due to obstruction

The loss of head due to obstruction in a pipe takes place due to reduction in the cross sectional area of the pipe by the presence of obstruction which is followed by an abrupt enlargement of the stream lines beyond the obstruction. (Shown in figure)


Let, $\mathrm{V}=$ Velocity of fluid in pipe
$\mathrm{A} 0=$ Maximum area of obstruction
$\mathrm{A}=$ Area of pipe
ho $=$ head loss due to obstruction

$$
\mathrm{h}_{0}=\left[\frac{1}{c c(A-A o)}-1\right]^{2} \frac{V^{2}}{2 g}
$$

PROBLEM 1. At a sudden enlargement of a water main from 240 mm to 480 mm diameter, the hydraulic gradient rises by 10 mm . Estimate the rate of flow.

Given: Dia. of smaller pipe $\mathrm{D} 1=240 \mathrm{~mm}=0.24 \mathrm{~m}$

$$
\text { Area } \mathrm{A}_{1}=\frac{\pi}{4} \mathrm{D}_{1}^{2}=\frac{\pi}{4}(0.24)^{2}
$$

Dia. of larger pipe $\mathrm{D} 2=480 \mathrm{~mm}=0.48 \mathrm{~m}$

$$
\text { Area } \mathrm{A}_{2}=\frac{\pi}{4} D_{2}^{2}=\frac{\pi}{4}(0.48)^{2}
$$

Rise of hydraulic gradient i.e. $Z_{2}+\frac{P_{2}}{\rho g}-Z_{1}+\frac{P_{1}}{\rho g}=10 \mathrm{~mm}=\frac{10}{1000} m=\frac{1 \mathrm{~m}}{100}$
Let the rate of flow $=\mathrm{Q}$
Applying Bernoulli's equation to both sections i.e smaller and larger sections
$\frac{\mathrm{P}_{1}}{\rho \mathrm{~g}}+\frac{\mathrm{V}_{1}{ }^{2}}{2 \mathrm{~g}}+\mathrm{Z} \underset{1}{ }=\frac{\mathrm{P}_{2}}{\rho \mathrm{\rho g}}+\frac{\mathrm{V}_{2}{ }^{2}}{2 \mathrm{~g}}+\mathrm{Z}_{2}+$ Head loss due to enlargement $\qquad$
But head loss due to enlargement, he $=\frac{\mathrm{V}_{1}-\mathrm{V}_{2}{ }^{2}}{2 \mathrm{~g}}$
From continuity equation, we have $\mathrm{A}_{1} \mathrm{~V}_{1}=\mathrm{A}_{2} \mathrm{~V}_{2} \quad V_{1}=\frac{\mathrm{A}_{2} \mathrm{~V}_{2}}{\mathrm{~V}_{1}}$

$$
V_{1}=\frac{\frac{\pi}{4} D_{2}^{2} V_{2}}{\frac{\pi}{4} D_{1}^{2}}={\frac{D_{2}}{D_{1}}}^{2} \times V_{2}={\frac{0.48^{2}}{0.24} \quad V_{2}=2^{2} V_{2}=4 V_{2}}_{V_{1}}
$$

Substituting this value in equation (2), we get

$$
\text { he }={\frac{4 V_{2}-V_{2}}{2 g}}^{2}={\frac{3 V_{2}}{2 g}}^{2}=\frac{9 V_{2}^{2}}{2 g}
$$

Now substituting the value of he and V1 in equation (1)

$$
\begin{aligned}
& \frac{\mathrm{P}_{1}}{\rho g}+\frac{4 V_{2}^{2}}{2 \mathrm{~g}}+Z_{1}=\frac{\mathrm{P}_{2}}{\rho \mathrm{~g}}+\frac{\mathrm{V}_{2}^{2}}{2 \mathrm{~g}}+\mathrm{Z}_{2}+\frac{9 V_{2}^{2}}{2 g} \\
& \frac{16 \mathrm{~V}_{2}^{2}}{2 \mathrm{~g}}-\frac{\mathrm{V}_{2}^{2}}{2 \mathrm{~g}}-\frac{9 V_{2}^{2}}{2 g}=\frac{\mathrm{P}_{2}}{\rho \mathrm{~g}}+\mathrm{Z}_{2}-\frac{\mathrm{P}_{1}}{\rho \mathrm{~g}}+Z_{1}
\end{aligned}
$$

But Hydraulic gradient rise $=\frac{\mathrm{P}_{2}}{\rho g}+Z_{2}-\frac{\mathrm{P}_{1}}{\rho g}+Z_{1}=\frac{1}{100} \mathrm{~m}$
$\frac{6 \mathrm{~V}_{2}{ }^{2}}{2 \mathrm{~g}}=\frac{1}{100} \mathrm{~m} \quad V_{2}=\frac{2 \times 9.81}{6 \times 100}=0.1808=0.181 \mathrm{~m} / \mathrm{sec}$
Discharge

$$
\begin{aligned}
\mathrm{Q} & =\mathrm{A}_{2} \mathrm{~V}_{2}=\frac{\pi}{4} \mathrm{D}_{2}^{2} \mathrm{~V}_{2} \\
& =\frac{\pi}{4}(0.48)^{2} \times 0.181=0.03275 \mathrm{~m}^{3} / \mathrm{sec} \\
& =32.75 \mathrm{Lts} / \mathrm{sec}
\end{aligned}
$$

PROBLEM 2. A 150 mm dia. pipe reduces in dia. abruptly to 100 mm dia. If the pipe carries water at $301 \mathrm{lts} / \mathrm{sec}$, calculate the pressure loss across the contraction. Take coefficient of contraction as 0.6.

Given: Dia. of larger pipe $\mathrm{D} 1=150 \mathrm{~mm}=0.15 \mathrm{~m}$
Area of larger pipe $A_{1}=\frac{\pi}{4}(0.15)^{2}=0.01767 \mathrm{~m}^{2}$
Dia. of smaller pipe $\mathrm{D} 2=100 \mathrm{~mm}=0.10 \mathrm{~m}$
Area of smaller pipe $\mathrm{A}_{2}=\frac{\pi}{4}(0.10)^{2}=0.007854 \mathrm{~m}^{2}$
Discharge $\mathrm{Q}=30$ lts $/ \mathrm{sec}=0.03 \mathrm{~m} 3 / \mathrm{sec}$ Co-efficient of contraction $\mathrm{CC}=0.6$
From continuity equation, we have $\mathrm{Q}=\mathrm{A} 1 \mathrm{~V} 1=\mathrm{A} 2 \mathrm{~V} 2$

$$
\begin{aligned}
& V_{1}=\frac{Q}{A_{1}}=\frac{0.03}{0.01767}=1.697 \mathrm{~m} / \mathrm{sec} \\
& V_{2}=\frac{Q}{A_{2}}=\frac{0.03}{0.007854}=3.82 \mathrm{~m} / \mathrm{sec}
\end{aligned}
$$

Applying Bernoulliees equation before and after contraction

$$
\begin{equation*}
\frac{\mathrm{P}_{1}}{\rho g}+\frac{\mathrm{V}_{1}{ }^{2}}{2 \mathrm{~g}}+\mathrm{Z}_{1}=\frac{\mathrm{P}_{2}}{\rho g}+\frac{\mathrm{V}_{2}{ }^{2}}{2 \mathrm{~g}}+\mathrm{Z}_{2}+\mathrm{h}_{\mathrm{c}} \tag{1}
\end{equation*}
$$

But $\mathrm{Z} 1=\mathrm{Z} 2$ and hc the head loss due to contraction is given by the equation

$$
\mathrm{hc}=\left(\frac{1}{c_{c}}-1\right)^{2} \frac{v_{2}^{2}}{2 g}=\frac{3.82^{2}}{2 \times 9.81}\left(\frac{1}{0.6}-1\right)^{2}=0.33
$$

Substituting these values in equation (1), we get

$$
\frac{P_{1}}{\rho g}+\frac{1.697^{2}}{2 \times 9.81}=\frac{P_{2}}{\rho g}+\frac{3.82^{2}}{2 \times 9.81}+0.33
$$

$$
\frac{P_{1}}{\rho g}+0.1467=\frac{P_{2}}{\rho g}+0.7438+0.33
$$

$$
\frac{P_{1}}{\rho g}-\frac{P_{2}}{\rho g}=0.7438+0.33-0.1467=0.9271 \mathrm{~m} \text { of } \text { Water }
$$

$$
\begin{aligned}
P_{1}-P_{2} & =\rho g \times 0.9271=1000 \times 9.81 \times 0.9271=0.909 \times 10^{4} \mathrm{~N} / \mathrm{m}^{2} \\
& =0.909 \mathrm{~N} / \mathrm{cm}^{2}
\end{aligned}
$$

Pressure loss across contraction $=P 1-P 2=0.909 \mathrm{~N} / \mathrm{cm}^{2}$
PROBLEM 3. Water is flowing through a horizontal pipe of diameter 200 mm at a velocity of $3 \mathrm{~m} / \mathrm{sec}$. A circular solid plate of diameter 150 mm is placed in the pipe to obstruct the flow. Find the loss of head due to obstruction in the pipe, if $\mathrm{C}_{\mathrm{C}}=0.62$.

Given: Diameter of pipe $D=200 \mathrm{~mm}=$
$0.2 \mathrm{mVelocity} \mathrm{V}=3 \mathrm{~m} / \mathrm{sec}$

$$
\text { Area of pipe } A=\frac{\pi}{4} D^{2}=\frac{\pi}{4}(0.2)^{2}=0.03141 \mathrm{~m}^{2}
$$

Diameter of obstruction $d=150 \mathrm{~mm}=0.15 \mathrm{~m}$

$$
\text { Area of obstruction } \mathrm{a}=\frac{\pi}{4}(0.15)^{2}=0.01767 \mathrm{~m}
$$

$$
\mathrm{C}_{\mathrm{C}}=0.62
$$

The head loss due to obstruction

$$
\begin{aligned}
\mathrm{h}_{\mathrm{o}} & =\left[\frac{1}{c c(A-A o)}-1\right]^{2} \frac{V^{2}}{2 g} \\
& =\frac{9}{19.62}[3.687-1]^{2} \\
& =3.311 \mathrm{~m}
\end{aligned}
$$

## 6 PIPES IN SERIES AND IN PARALLEL

## PIPES IN SERIES:

When pipes of different lengths and different diameters are connected end to end to form a pipe line, such arrangement or connection of pipes will be considered as pipes in series or compound pipes. Following figure, displayed here, indicates the arrangement of connection of three pipes in series.


Let us consider the following terms from above figure
$L_{1}, L_{2}$ and $L_{3}$ : Length of pipes 1,2 and 3 respectively $\mathrm{d}_{1}, \mathrm{~d}_{2}$ and $\mathrm{d}_{3}$ : Diameter of pipes 1,2 and 3 respectively $\mathrm{V}_{1}$, $V_{2}$ and $V_{3}$ : Velocity of flow through pipes 1, 2 and 3 respectively
$f_{1}, f_{2}$ and $f_{3}$ : Co-efficient of friction for pipes 1,2 and 3 respectively
$\mathrm{H}=$ Difference of water level in two tanks

We must note it here that difference in liquid surface level will be equal to the sum of total head loss in the pipes.

If we neglect the minor head losses, we will have following equation for total head loss as mentioned here.

$$
H=\frac{4 f_{1} L_{1} V_{1}^{2}}{d_{1} \times 2 g}+\frac{4 f_{2} L_{2} V_{2}^{2}}{d_{2} \times 2 g}+\frac{4 f_{3} L_{3} V_{3}^{2}}{d_{3} \times 2 g}
$$

Let us consider that co-efficient of friction i.e. $f$ is same for all three pipes and therefore we can write the equation for head loss as mentioned here.

$$
\begin{aligned}
H & =\frac{4 f L_{1} V_{1}^{2}}{d_{1} \times 2 g}+\frac{4 f L_{2} V_{2}^{2}}{d_{2} \times 2 g}+\frac{4 f L_{3} V_{3}^{2}}{d_{3} \times 2 g} \\
& =\frac{4 f}{2 g}\left[\frac{L_{1} V_{1}^{2}}{d_{1}}+\frac{L_{2} V_{2}^{2}}{d_{2}}+\frac{L_{3} V_{3}^{2}}{d_{3}}\right]
\end{aligned}
$$

## PIPES IN PARALLEL:

When a main pipeline divides in to two or more parallel pipes, which may again join together downstream and continue as main line, the pipes are said to be in parallel. The pipes are connected in parallel in order to increase the discharge passing through the
 main.
It is analogous to parallel electric current in which the drop in potential and flow of electric current can be compared to head loss and rate of discharge in a fluid flow respectively.
The rate of discharge in the main line is equal to the sum of the discharges in each of the parallel pipes.

$$
\text { Thus } \mathrm{Q}=\mathrm{Q} 1+\mathrm{Q} 2
$$

The flow of liquid in pipes (1) and (2) takes place under the difference of head between the sections $A$ and $B$ and hence the loss of head between the sections $A$ and $B$ will be the same whether the liquid flows through pipe (1) or pipe (2). Thus if $\mathrm{D}_{1}, \mathrm{D}_{2}$ and $\mathrm{L}_{1}, \mathrm{~L}_{2}$ are the diameters and lengths of the pipes (1) and (2) respectively, then the velocities of flow $V_{1}$ and $V_{2}$ in the two pipes must be such as to give

$$
\begin{aligned}
\frac{4 f_{1} L_{1} V_{1}^{2}}{d_{1} \times 2 g} & =\frac{4 f_{2} L_{2} V_{2}^{2}}{d_{2} \times 2 g} \\
f_{1} & =f_{2}, \text { then } \frac{L_{1} V_{1}^{2}}{d_{1} \times 2 g}=\frac{L_{2} V_{2}^{2}}{d_{2} \times 2 g}
\end{aligned}
$$

## EQUIVALENT PIPE

In practice adopting pipes in series may not be feasible due to the fact that they may be of unistandard size (ie. May not be comemercially available) and they experience other minor losses. Hence, the entire system will be replaced by a single pipe of uniform diameter D , but of the same length $\mathrm{L}=\mathrm{L}_{1}+\mathrm{L}_{2}+\mathrm{L}_{3}$ such that the head loss due to friction for both the pipes, viz equivalent pipe $\&$ the compound pipe are the same.

For a compound pipe or pipes in series

$$
\begin{aligned}
& h_{f}=h f_{1}+h f_{2}+h f_{3} \\
& h_{f}=\frac{8 f L_{1} Q^{2}}{g \pi^{2} D_{1}^{5}}+\frac{8 f L_{2} Q^{2}}{g \pi^{2} D_{2}^{5}}+\frac{8 f L_{3} Q^{2}}{g \pi^{2} D_{3}^{5}}---(1)
\end{aligned}
$$

for an equivalent pipe $h_{f}=\frac{8 f L Q^{2}}{g \pi^{2} D^{5}}---(2)$
Equating (1) \& (2) and simplifying $\frac{L}{D^{5}}=\frac{L_{1}}{D_{1}^{5}}+\frac{L_{2}}{D_{2}^{5}}+\frac{L_{3}}{D_{3}^{5}}$
or

$$
D=\left\{\frac{L}{\frac{L_{1}}{D_{1}^{5}}+\frac{L_{2}}{D_{2}^{5}}+\frac{L_{3}}{D_{3}^{5}}}\right\}^{\frac{1}{5}}
$$

PROBLEM 1:The difference in water surface levels in two tanks, which are connected by three pipes in series of lengths $400 \mathrm{~m}, 200 \mathrm{~m}$ and 300 m and of diameters 400 mm , 300 mm and 200 mm respectively, is 16 m . Estimate the rate of flow of water if coefficient of friction for these pipes is same and equal to 0.005 , considering: (i) minor losses also (ii) neglecting minor losses.

Solution. Given :
Difference of water levels, $H=16 \mathrm{~m}$
Length and dia. of pipe $1, L_{1}=400 \mathrm{~m}$ and $d_{1}=400 \mathrm{~mm}=0.4 \mathrm{~m}$
Length and dia. of pipe 2, $L_{2}=200 \mathrm{~m}$ and $d_{2}=200 \mathrm{~mm}=0.2 \mathrm{~m}$ Length and dia. of pipe 3, $L_{3}=300 \mathrm{~m}$ and $d_{3}=300 \mathrm{~mm}=0.3 \mathrm{~m}$ Also

$$
f_{1}=f_{2}=f_{3}=0.005
$$

(i) Discharge through the compound pipe first neglecting minor losses.

Let $V_{1}, V_{2}$ and $V_{3}$ are the velocities in the 1st, 2nd and 3rd pipe respectively.
From continuity, we have $A_{1} V_{1}=A_{2} V_{2}=A_{3} V_{3}$

$$
\begin{aligned}
& V_{2}=\frac{A_{1} V_{1}}{A_{2}}=\frac{\frac{\pi}{4} d_{1}^{2}}{\frac{\pi}{4} d_{2}^{2}} \times V_{1}=\frac{d_{1}^{2}}{d_{2}^{2}} V_{1}=\left(\frac{0.4}{0.2}\right)^{2} V_{1}=4 V_{1} \\
& V_{3}=\frac{A_{1} V_{1}}{A_{3}}=\frac{\frac{\pi}{4} d_{1}^{2}}{\frac{\pi}{4} d_{3}^{2}} \times V_{1}=\frac{d_{1}^{2}}{d_{3}^{2}} V_{1}=\left(\frac{0.4}{0.2}\right)^{2} V_{1}=1.77 V_{1} \\
& \qquad H=\frac{4 f_{1} L_{1} V_{1}^{2}}{d_{1} \times 2 g}+\frac{4 f_{2} L_{2} V_{2}^{2}}{d_{2} \times 2 g}+\frac{4 f_{3} L_{3} V_{3}^{2}}{d_{3} \times 2 g} \\
& 16= \\
& =\frac{4 \times 0.005 \times 400 \times V_{1}^{2}}{0.4 \times 2 \times 9.81}+\frac{4 \times 0.005 \times 200 \times\left(4 V_{1}\right)^{2}}{0.2 \times 2 \times 9.81}+\frac{4 \times 0.005 \times 300}{0.3 \times 2 \times 9.81} \times\left(1.77 V_{1}\right)^{2} \\
& 2 \times 9.81 \\
& V_{1}^{2} \\
& \left.\hline \frac{4 \times 0.005 \times 400}{0.4}+\frac{4 \times 0.005 \times 200 \times 16}{0.2}+\frac{4 \times 0.005 \times 300 \times 3.157}{0.3}\right)
\end{aligned}
$$

$$
\begin{gathered}
16= \\
\frac{V_{1}^{2}}{2 \times 9.81}(20+320+63.14)=\frac{V_{1}^{2}}{2 \times 9.81} \times 403.14 \\
\therefore \quad V_{1}=\sqrt{\frac{16 \times 2 \times 9.81}{403.14}}=0.882 \mathrm{~m} / \mathrm{s}
\end{gathered}
$$

$\therefore$ Discharge,

$$
Q=A_{1} \times V_{1}=\frac{\pi}{4}(0.4)^{2} \times 0.882=\mathbf{0 . 1 1 0 8} \mathrm{m}^{3} / \mathrm{s}
$$

(ii) Discharge through the compound pipe considering minor losses also.

Minor losses are :
(a) At inlet,

$$
h_{i}=\frac{0.5 V_{1}^{2}}{2 g}
$$

(b) Between 1st pipe and 2nd pipe, due to contraction,

$$
h_{c}=\frac{0.5 V_{2}^{2}}{2 g}=\frac{0.5\left(4 V_{1}^{2}\right)}{2 g} \quad\left(\because V_{2}=4 V_{1}\right)
$$

$$
=\frac{0.5 \times 16 \times V_{1}^{2}}{2 g}=8 \times \frac{V_{1}^{2}}{2 g}
$$

(c) Between 2nd pipe and 3rd pipe, due to sudden enlargement,

$$
\begin{aligned}
h_{e} & =\frac{\left(V_{2}-V_{3}\right)^{2}}{2 g}=\frac{\left(4 V_{1}-1.77 V_{1}\right)^{2}}{2 g} \quad\left(\because V_{3}=1.77 V_{1}\right) \\
& =(2.23)^{2} \times \frac{V_{1}^{2}}{2 g}=4.973 \frac{V_{1}^{2}}{2 g}
\end{aligned}
$$

(d) At the outlet of 3rd pipe, $h_{o}=\frac{V_{3}^{2}}{2 g}=\frac{\left(1.77 V_{1}\right)^{2}}{2 g}=1.77^{2} \times \frac{V_{1}^{2}}{2 g}=3.1329 \frac{V_{1}^{2}}{2 g}$

The major losses are

$$
=\frac{4 f_{1} \times L_{1} \times V_{1}^{2}}{d_{1} \times 2 g}+\frac{4 f_{2} \times L_{2} \times V_{2}^{2}}{d_{2} \times 2 g}+\frac{4 f_{3} \times L_{3} \times V_{3}^{2}}{d_{3} \times 2 g}
$$

$=\frac{4 \times 0.005 \times 400 \times V_{1}^{2}}{0.4 \times 2 \times 9.81}+\frac{4 \times 0.005 \times 200 \times\left(4 V_{1}\right)^{2}}{0.2 \times 2 \times 9.81}+\frac{4 \times 0.005 \times 300 \times\left(1.77 V_{1}\right)^{2}}{0.3 \times 2 \times 9.81}$
$=403.14 \times \frac{V_{1}^{2}}{2 \times 9.81}$
$\therefore$ Sum of minor losses and major losses

$$
=\left[\frac{0.5 V_{1}^{2}}{2 g}+8 \times \frac{V_{1}^{2}}{2 g}+4.973 \frac{V_{1}^{2}}{2 g}+3.1329 \frac{V_{1}^{2}}{2 g}\right]+403.14 \frac{V_{1}^{2}}{2 g}
$$

$$
=419.746 \frac{V_{1}^{2}}{2 g}
$$

But total loss must be equal to $H$ (or 16 m )

$$
\therefore \quad 419.746 \times \frac{V_{1}^{2}}{2 g}=16 \quad \therefore \quad V_{1}=\sqrt{\frac{16 \times 2 \times 9.81}{419.746}}=0.864 \mathrm{~m} / \mathrm{s}
$$

$\therefore$ Discharge,$\quad Q=A_{1} V_{1}=\frac{\pi}{4}(0.4)^{2} \times 0.864=\mathbf{0 . 1 0 8 5} \mathbf{~ m}^{3} / \mathrm{s}$.

PROBLEM 2:Three pipes of length $800 \mathrm{~m}, 500 \mathrm{~m}$ and 400 m of diameter $500 \mathrm{~mm}, 400 \mathrm{~mm}$ and 300 mm respectively are connected are connected in series these pipes are to be replaced by a single pipe of length 1700 m.find the diameter of single pipe.

Solution. Given :
Length of pipe 1 ,
Length of pipe 2,
Length of pipe 3,
$L_{1}=800 \mathrm{~m}$ and dia., $d_{1}=500 \mathrm{~mm}=0.5 \mathrm{~m}$
$L_{2}=500 \mathrm{~m}$ and dia., $d_{2}=400 \mathrm{~mm}=0.4 \mathrm{~m}$
$L_{3}=400 \mathrm{~m}$ and dia., $d_{3}=300 \mathrm{~mm}=0.3 \mathrm{~m}$ $L=1700 \mathrm{~m}$

Let the diameter of equivalent single pipe $=d$

$$
\frac{L}{d^{5}}=\frac{L_{1}}{d_{1}^{5}}+\frac{L_{2}}{d_{2}^{5}}+\frac{L_{3}}{d_{3}^{5}}
$$

$$
\frac{1700}{d^{5}}=\frac{800}{.5^{5}}+\frac{500}{.4^{5}}+\frac{400}{0.3^{5}}
$$

$$
=25600+48828.125+164609=239037
$$

$$
\therefore \quad d^{5}=\frac{1700}{239037}=.007118
$$

$$
\therefore \quad d=(.007188)^{0.2}=0.3718=\mathbf{3 7 1 . 8} \mathbf{~ m m} .
$$

