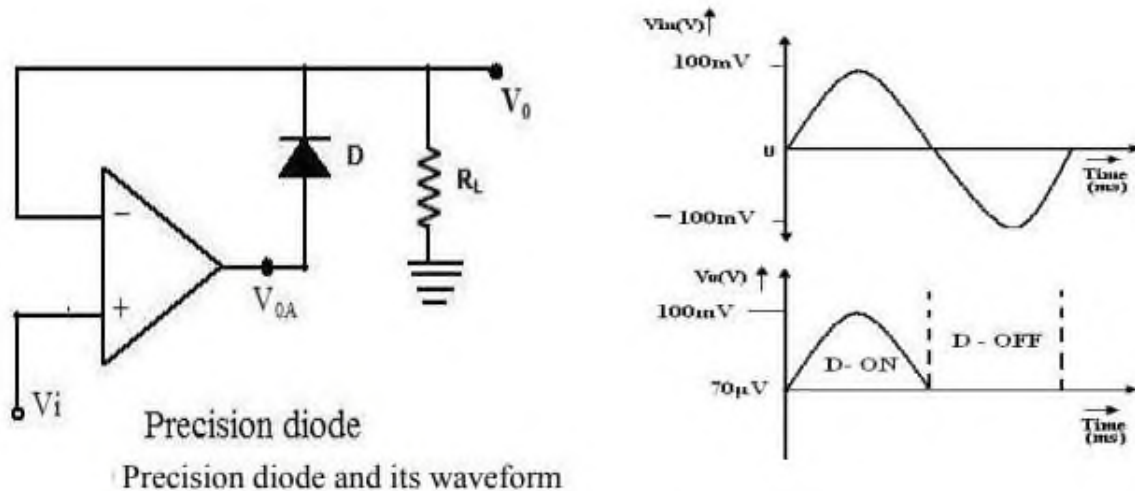


## Precision Rectifier:

The ordinary diodes cannot rectify voltages below the cut-in voltage of the diode. A circuit which can act as an ideal diode or precision signal – processing rectifier circuit for rectifying voltages which are below the level of cut-in voltage of the diode can be designed by placing the diode in the feedback loop of an op-amp.



## Precision diodes:

Figure shows the arrangement of a precision diode. It is a single diode arrangement and functions as a non-inverting precision half-wave rectifier circuit. If  $V_i$  in the circuit of figure is positive, the op-amp output  $V_{OA}$  also becomes positive. Then the closed loop condition is achieved for the op-amp and the output voltage  $V_0 = V_i$ . When  $V_i < 0$ , the voltage  $V_{OA}$  becomes negative and the diode is reverse biased. The loop is then broken and the output  $V_0 = 0$ . Consider the open loop gain AOL of the op-amp is approximately  $10^4$  and the cut-in voltage  $V_\gamma$  for silicon diode is  $\approx 0.7V$ . When the input voltage  $V_i > V_\gamma / AOL$ , the output of the op-amp  $V_{OA}$  exceeds  $V_\gamma$  and the diode D conducts.

Then the circuit acts like a voltage follower for input voltage level  $V_i > V_\gamma / AOL$ , (i.e. when  $V_i > 0.7/10^4 = 70\mu V$ ), and the output voltage  $V_0$  follows the input voltage during the positive half cycle for input voltages higher than  $70\mu V$  as shown in figure.

When  $V_i$  is negative or less than  $V_\gamma / AOL$ , the output of op-amp  $V_{OA}$  becomes negative, and the diode becomes reverse biased. The loop is then broken, and the op-amp swings down to negative saturation. However, the output terminal is now isolated from both the input signal and the output of the op-amp terminal thus  $V_0 = 0$ .

No current is then delivered to the load  $R_L$  except for the small bias current of the op-amp and the reverse saturation current of the diode.

This circuit is an example of a non-linear circuit, in which linear operation is achieved over the remaining region ( $V_i < 0$ ). Since the output swings to negative saturation level when  $V_i < 0$ , the circuit is basically of saturating form. Thus the frequency response is also limited.

**Applications:** The precision diodes are used in

- half wave rectifier,
- Full-wave rectifier,

- peak value detector,
- Clipper and clamper circuits.

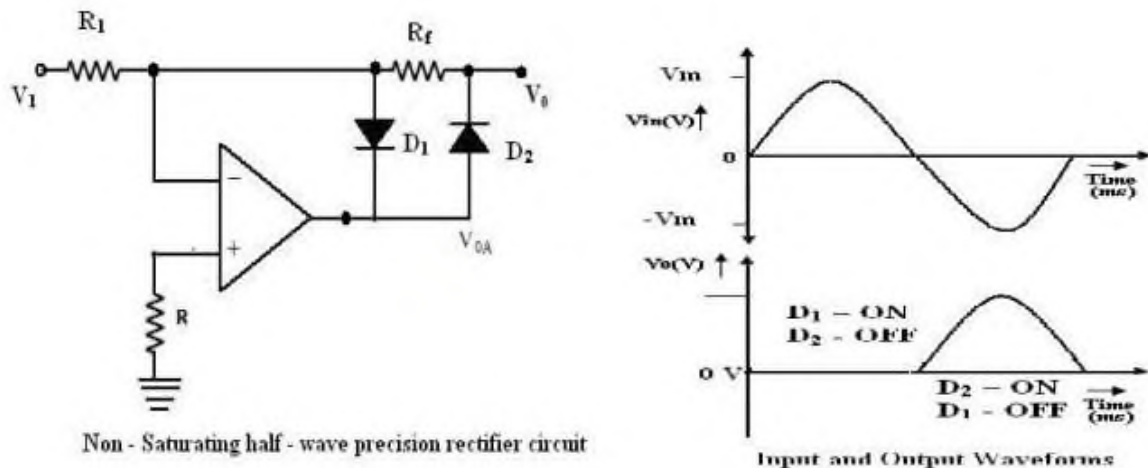
**Disadvantage:**

It can be observed that the precision diode as shown in figure operated in the first quadrant with  $V_i > 0$  and  $V_o > 0$ . The operation in third quadrant can be achieved by connecting the diode in reverse direction.

**Half – wave Rectifier:**

A non-saturating half wave precision rectifier circuit is shown in figure. When  $V_i > 0V$ , the voltage at the inverting input becomes positive, forcing the output  $V_{OA}$  to go negative. This results in forward biasing the diode  $D_1$  and the op-amp output drops only by  $\approx 0.7V$  below the inverting input voltage. Diode  $D_2$  becomes reverse biased. The output voltage  $V_o$  is zero when the input is positive.

When  $V_i < 0$ , the op-amp output  $V_{OA}$  becomes positive, forward biasing the diode  $D_2$  and reverse biasing the diode  $D_1$ . The circuit then acts like an inverting amplifier circuit with a non-linear diode in the forward path. The gain of the circuit is unity when  $R_f = R_i$ .



**Half wave rectifier and its operation**

The circuit operation can mathematically be expressed as  
 $V_o = 0$  when  $V_i > 0$  and  
 $V_o = R_f/R_i V_i$  for  $V_i < 0$

The voltage  $V_{oA}$  at the op amp output is  $V_{oA} = -0.7V$  for  $V_i > 0$   
 $V_{oA} = R_f/R_i V_i + 0.7V$  for  $V_i < 0$

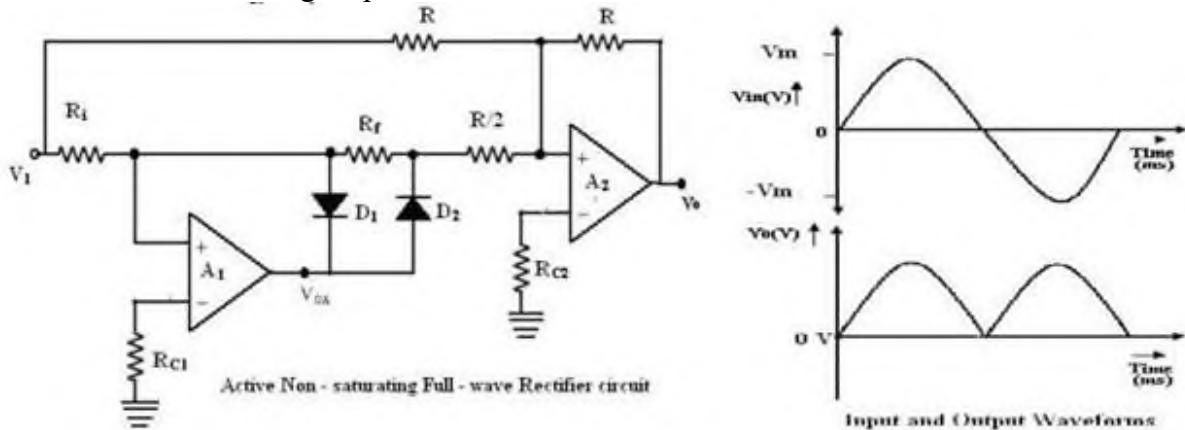
**Advantages:**

- It is a precision half wave rectifier and
- It is a non saturating one.

The inverting characteristics of the output  $V_o$  can be circumvented by the use of an additional inversion for achieving a positive output.

**Full wave Rectifier:**

The first part of the Full wave circuit is a half wave rectifier circuit. The second part of the circuit is an inverting amplifier.



**Full wave rectifier and its operation**

For positive input voltage  $V_i > 0V$  and assuming that  $R_F = R_i = R$ , the output voltage  $V_{OA} = V_i$ . The voltage  $V_0$  appears as (-) input to the summing op-amp circuit formed by  $A_2$ , The is  $R/(R/2)$ , as shown in figure.

The input  $V_i$  also appears as an input to the summing amplifier. Then, the net output is  $V_0 = -V_i - 2V_0 = -V_i - 2(-V_i) = V_i$ . Since  $V_i > 0V$ ,  $V_0$  will be positive, with its input output characteristics in first quadrant. For negative input  $V_i < 0V$ , the output  $V_0$  of the first part of rectifier circuit is zero. Thus, one input of the summing circuit has a value of zero. However,  $V_i$  is also applied as an input to the summer circuit formed by the op-amp  $A_2$ .

The gain for this input is  $(-R/R) = -1$ , and hence the output is  $V_0 = -V_i$ . Since  $V_i$  is negative,  $V_0$  will be inverted and will thus be positive. This corresponds to the second quadrant of the circuit.

To summarize the operation of the circuit,

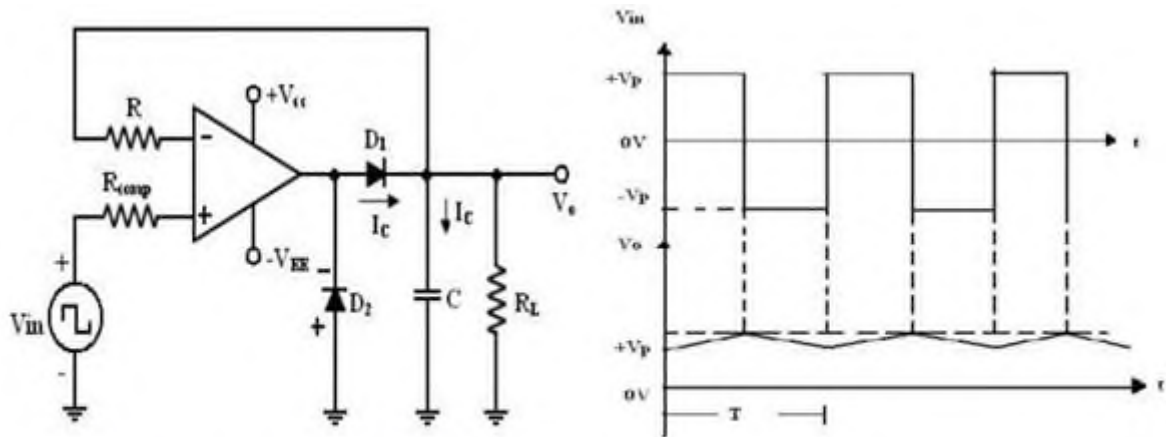
$V_0 = V_i$  when  $V_i < 0V$  and

$V_0 = V_i$  for  $V_i > 0V$ , and hence

$V_0 = |V_i|$

**Peak Detector**

Square, Triangular, Saw tooth and pulse waves are typical examples of non-sinusoidal waveforms. A conventional AC voltmeter cannot be used to measure these sinusoidal waveforms because it is designed to measure the RMS value of the pure sine wave. One possible solution to this problem is to measure the peak values of the non-sinusoidal waveforms. Peak detector measures the +ve peak value of the square wave input.



Peak detector circuit and input and output waveforms

- i) During the positive half cycle of  $V_{in}$ : the o/p of the op-amp drives  $D_1$  on. (Forward biased) Charging capacitor  $C$  to the positive peak value  $V_p$  of the input volt  $V_{in}$ .
- ii) During the negative half cycle of  $V_{in}$ :  $D_1$  is reverse biased and voltage across  $C$  is retained. The only discharge path for  $C$  is through  $R_L$  since the input bias  $I_B$  is negligible.

For proper operation of the circuit, the charging time constant ( $CR_d$ ) and discharging time constant ( $CR_L$ ) must satisfy the following condition.

$$CR_d \ll T/10$$

Where  $R_d$  = Resistance of the forward-biased diode.

$T$  = time period of the input waveform.

$$CR_L \gg 10T \quad (2)$$

Where  $R_L$  = load resistor.

If  $R_L$  is very small so that eqn. (2) cannot be satisfied.

- Use a (buffer) voltage follower circuit between capacitor  $C$  and  $R_L$  load resistor.
- $R$  is used to protect the op-amp against the excessive discharge currents.
- $R_{comp}$  = minimizes the offset problems caused by input current
- $D_2$  conducts during the  $-ve$  half cycle of  $V_{in}$  and prevents the op-amp from going into negative saturation.



## Clipper and clipper

### Applications:

Wave shaping circuits are commonly used in digital computers and communication such as TV and FM receiver. Wave shaping technique include clipping and clamping.

In op-amp clipper circuits a rectifier diode may be used to clip off a certain portion of the input signal to obtain a desired o/p waveform. The diode works as an ideal diode (switch) because when on, the voltage drop across the diode is divided by the open loop gain of the op-amp. When off (reverse biased) the diode is an open circuit. In an op-amp clamper circuits, however a predetermined dc level is deliberately inserted in the o/p volt. For this reason, the clamper is sometimes called a dc inverter.

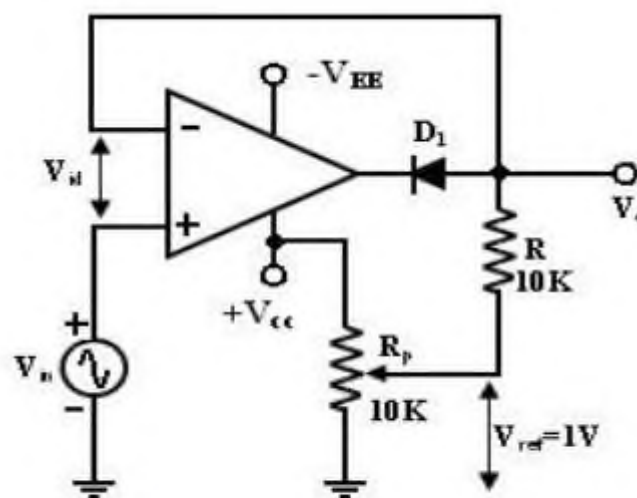
### Clipper: Positive Clipper:

A circuit that removes positive parts of the input signal can be formed by using an op-amp with a rectifier diode. The clipping level is determined by the reference voltage  $V_{ref}$ , which should less than the i/p range of the op-amp ( $V_{ref} < V_{in}$ ). The Output voltage has the portions of the positive half cycles above  $V_{ref}$  clipped off.

The circuit works as follows: During the positive half cycle of the input, the diode  $D_1$  conducts only until  $V_{in} = V_{ref}$ . This happens because when  $V_{in} < V_{ref}$ , the output volts  $V_0$  of the op-amp becomes negative to device  $D_1$  into conduction when  $D_1$  conducts it closes feedback loop and op-amp operates as a voltage follower. (i.e.) Output  $V_0$  follows input until  $V_{in} = V_{ref}$ .

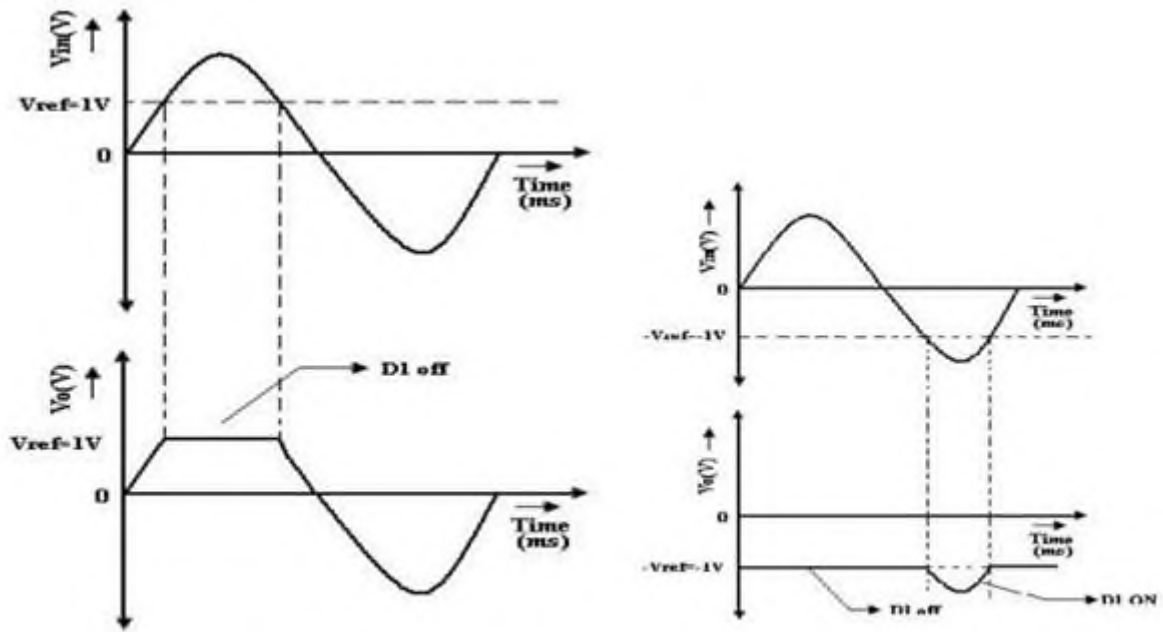
When  $V_{in} > V_{ref} \Rightarrow$  the  $V_0$  becomes +ve to derive  $D_1$  into off. It opens the feedback loop and op- amp operates open loop. When  $V_{in}$  drops below  $V_{ref}$  ( $V_{in} < V_{ref}$ ) the o/p of the op-amp  $V_0$  again becomes -ve to device  $D_1$  into conduction. It closes the feedback path. (o/p follows the i/p).

Thus diode  $D_1$  is on for  $v_{in} < V_{ref}$  (o/p follows the i/p) and  $D_1$  is off for  $V_{in} > V_{ref}$ . The op-amp alternates between open loop (off) and closed loop operation as the  $D_1$  is turned off and on respectively. For this reason the op-amp used must be high speed and preferably compensated for unity gain.



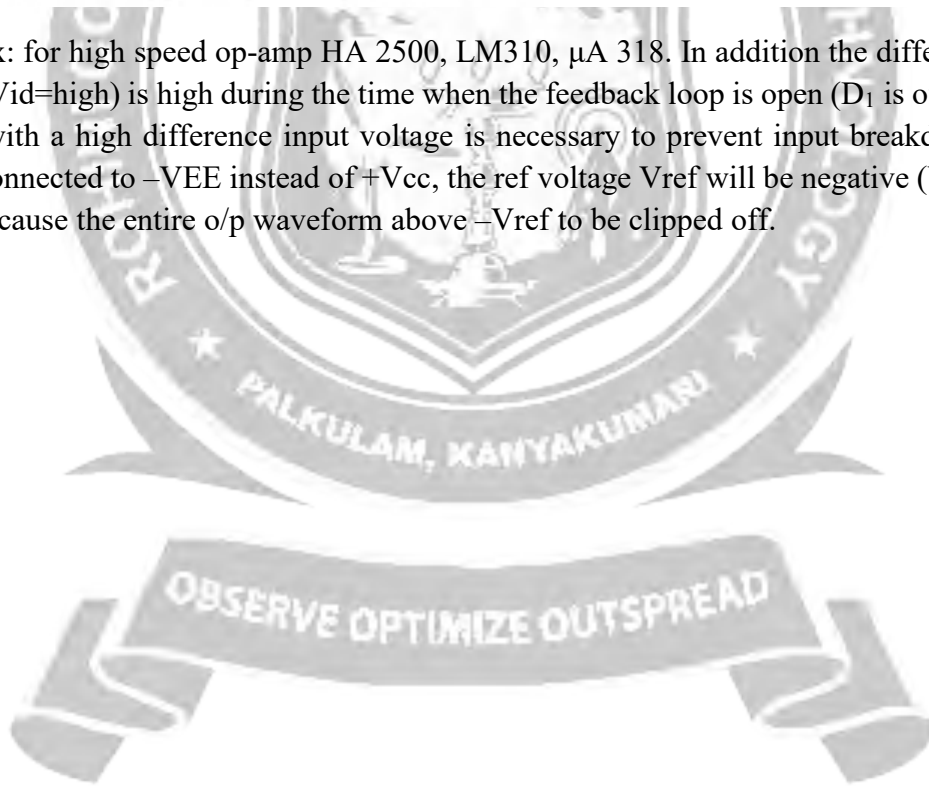
Positive Clipper



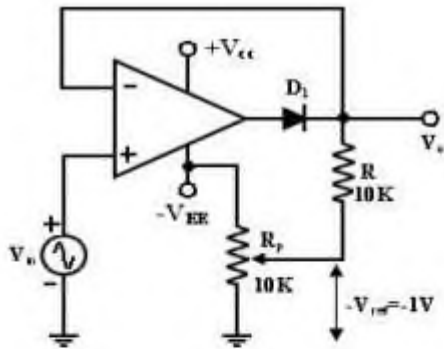


**Positive clipper input output waveforms**

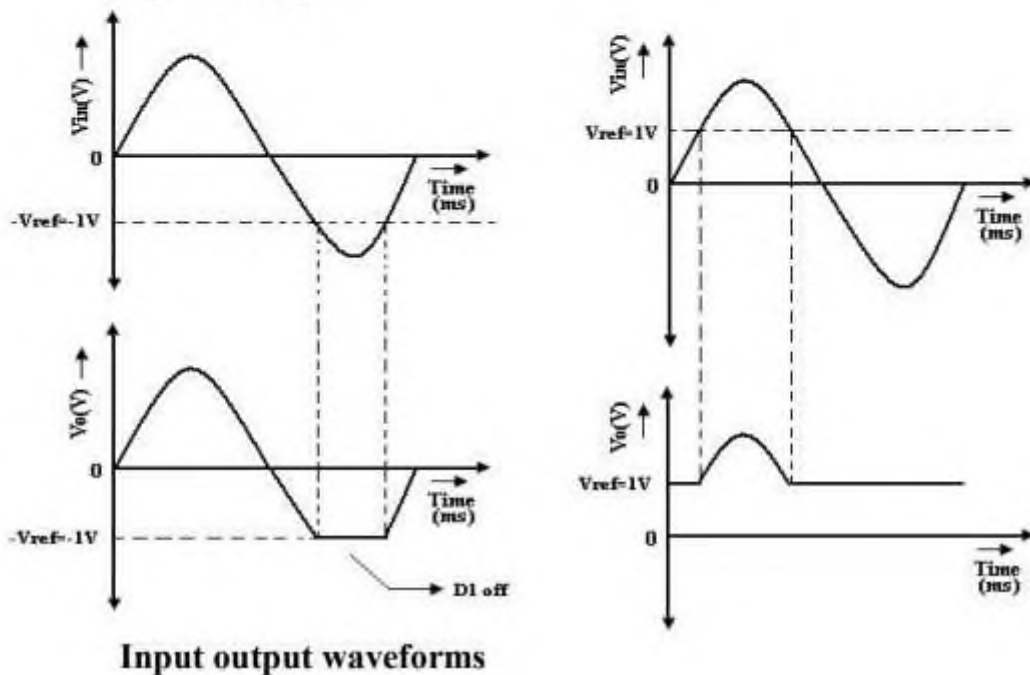
Ex: for high speed op-amp HA 2500, LM310,  $\mu A$  318. In addition the difference input voltage ( $V_{id} = \text{high}$ ) is high during the time when the feedback loop is open ( $D_1$  is off) hence an op-amp with a high difference input voltage is necessary to prevent input breakdown. If  $R_p$  (pot) is connected to  $-V_{EE}$  instead of  $+V_{CC}$ , the ref voltage  $V_{ref}$  will be negative ( $V_{ref} = -ve$ ). This will cause the entire o/p waveform above  $-V_{ref}$  to be clipped off.



**Negative Clipper:**



**Negative clipper**



**Input output waveforms**

The positive clipper is converted into a -ve clipper by simply reversing diode  $D_1$  and changing the polarity of  $V_{ref}$  voltage. The negative clipper clips off the -ve parts of the input signal below the reference voltage. Diode  $D_1$  conducts  $\rightarrow$  when  $V_{in} > -V_{ref}$  and therefore during this period o/p volt  $V_0$  follows the i/p volt  $V_{in}$ . The -ve portion of the output volt below  $-V_{ref}$  is clipped off because ( $D_1$  is off)  $V_{in} < -V_{ref}$ . If  $-V_{ref}$  is changed to  $+V_{ref}$  by connecting the potentiometer  $R_p$  to the  $+V_{cc}$ , the  $V_0$  below  $+V_{ref}$  will be clipped off. The diode  $D_1$  must be on for  $V_{in} > V_{ref}$  and off for  $V_{in}$ .

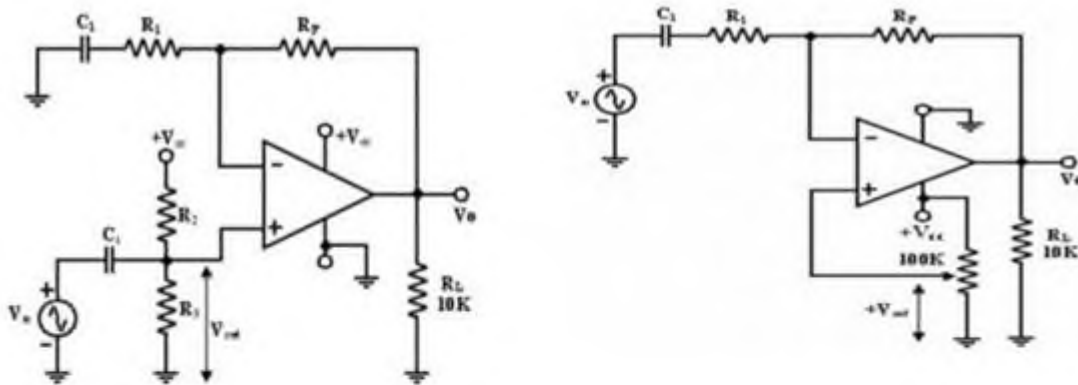
## CLAMPERS

### Positive and Negative Clampers:

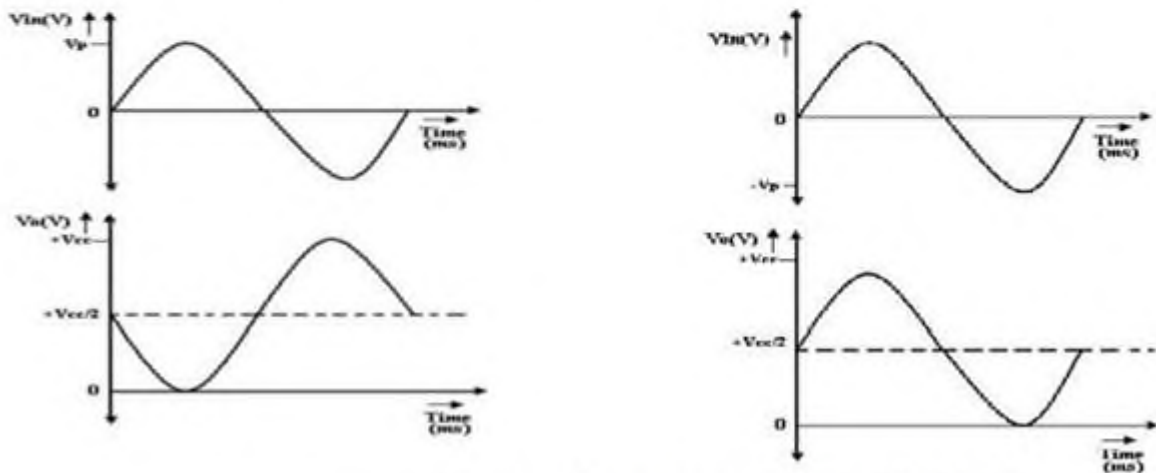
In clamper circuits a predetermined dc level is added to the output voltage. (or) The output is clamped to a desired dc level.

1. If the clamped dc level is +ve, the clamper is positive clamper
2. If the clamped dc level is -ve, the clamper is negative clamper.

Other equivalent terms used for clamper are dc inserter or restorer. Inverting and Non-Inverting that uses this technique.



### Positive -Negative campers



Input and output waveform with +Vref

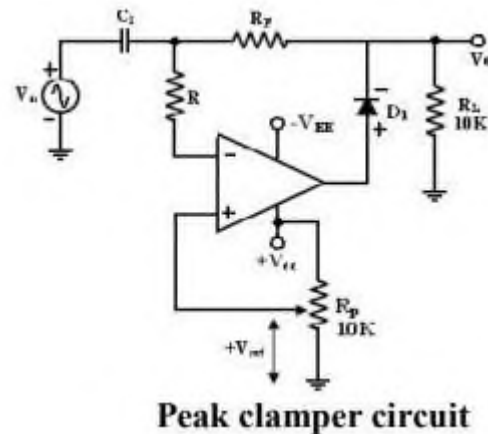
Capacitor:

The Value of the capacitors in these circuits depends on different input rates and pulse widths.

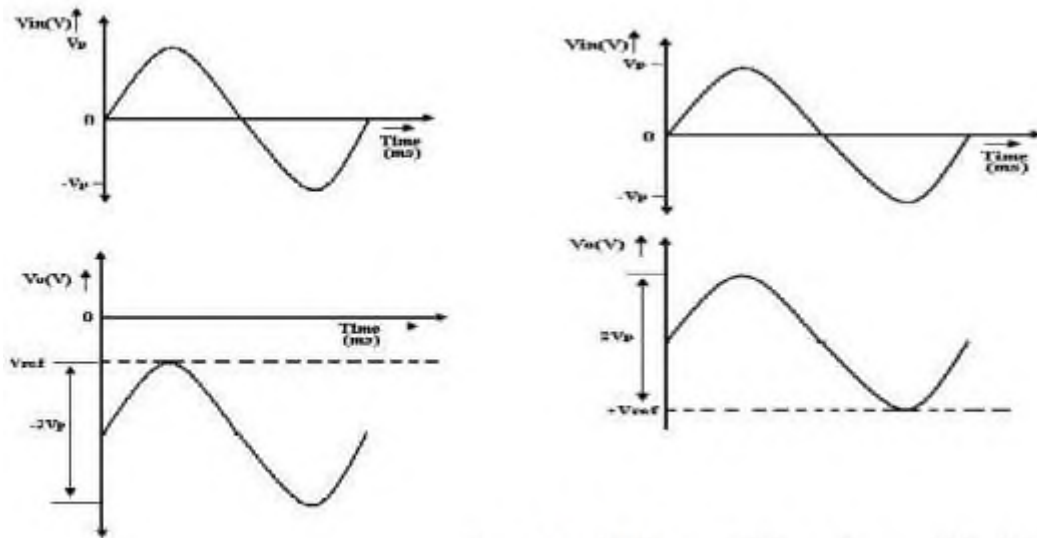
1. In both circuits the dc level added to the o/p voltage is approximately equal to  $V_{cc}/2$ .
2. This +ve fixed dc level is needed to obtain a maximum undistorted symmetrical sine wave.



**Peak clamper circuit:**



In this circuit, the input waveform peak is clamped at  $V_{ref}$ . For this reason, the circuit is called the peak clamper. First consider the input voltage  $V_{ref}$  at the (+) input: since this volt is +ve,  $V_o$  is also +ve which forward biases  $D_1$ . This closed the feedback loop. Voltage  $V_{in}$  at the (-) input: During its -ve half cycle, diode  $D_1$  conducts, charging  $c$ ; to the -ve peak value of  $V_p$ . During the +ve half cycle, diode  $D_1$  in reverse biased. Since this voltage  $V_p$  is in series with the +ve peak volt  $V_p$  the o/p volt  $V_o = 2 V_p$ . Thus the nett o/p is  $V_{ref}$  plus  $2 V_p$ . So the -ve peak of  $2 V_p$  is at  $V_{ref}$ . For precision clamping,  $C_i R_d \ll T/2$



**Input and Output Waveform with  $-V_{ref}$**

Where  $R_d$  = resistance of diode  $D_1$  when it is forward biased.

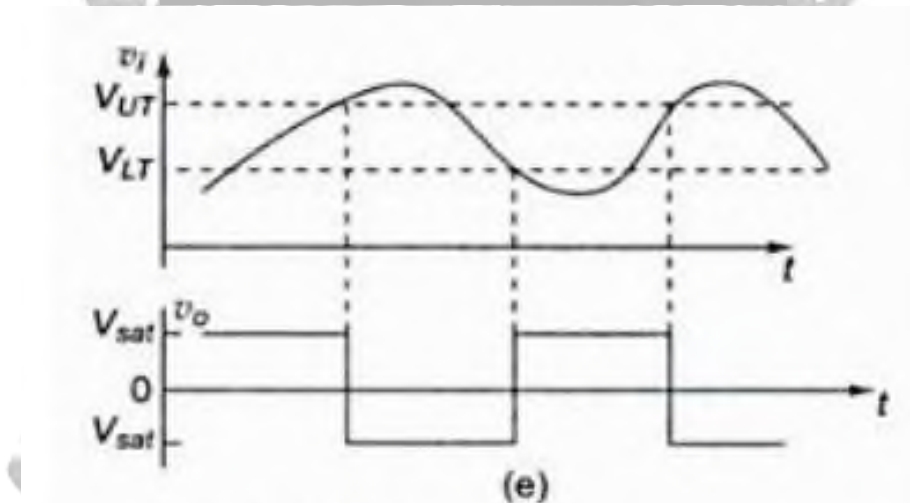
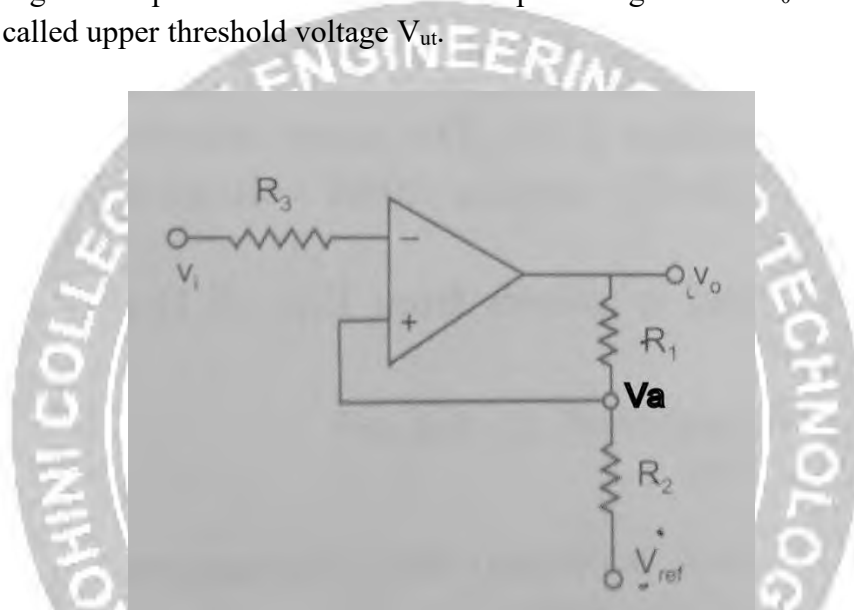
$T$  = time period of the input waveform.

Resistor  $R$  is used to protect the op-amp against excessive discharge currents from capacitor  $C_i$  especially when the dc supply voltages are switched off. A +ve peak clamping is accomplished by reversing  $D_1$  and using -ve reference voltage ( $-V_{ref}$ ).

### Schmitt Trigger: [Square Circuit]

This circuit converts an irregular shaped waveform to a square wave or pulse. The circuit is known as Schmitt Trigger or squaring circuit. The input voltage  $V_i$  triggers (changes the state of) the o/p  $V_o$  every time it exceeds certain voltage levels called the upper threshold  $V_{ut}$  and lower threshold voltage.

These threshold voltages are obtained by using the voltage divider  $R_1$ –  $R_2$ , where the voltage across  $R_1$  is feedback to the (+) input. The voltage across  $R_1$  is variable reference threshold voltage that depends on the value of the output voltage. When  $V_o = +V_{sat}$ , the voltage across  $R_1$  is called upper threshold voltage  $V_{ut}$ .



**Schmitt Trigger as squarer**

When  $V_o = +V_{sat}$ , the voltage across  $R_1$  is called upper threshold voltage  $V_{UT}$ .

$$V_{UT} = \frac{R_2 V_{ref} + R_1 V_{sat}}{R_1 + R_2}$$

- As long as  $V_i < V_{UT}$ , the output remains constant at  $+V_{sat}$ .
- When  $V_i > V_{UT}$ , the o/p regeneratively switches to  $-V_{sat}$ .

- When  $V_0 = -V_{sat}$ , the voltage across  $R_1$  is called lower threshold voltage  $V_{LT}$ .

$$V_{LT} = \frac{R_2 V_{ref}}{R_1 + R_2} - \frac{R_2 V_{sat}}{R_1 + R_2}$$

- The difference between the two threshold voltages are called hysteresis width .

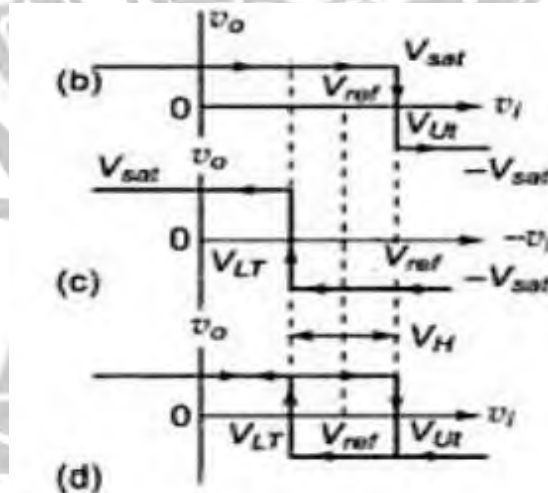
$$V_H = V_{UT} - V_{LT}$$

$$V_H = \frac{2R_2 V_{ref}}{R_1 + R_2}$$

- If  $V_{ref}$  is chosen as zero ,then

$$V_{UT} = -V_{LT} = \frac{2R_2 V_{sat}}{R_1 + R_2}$$

- If the threshold voltages  $V_{UT}$  and  $V_{LT}$  are made larger than the input noise voltages, the positive feedback will eliminate the false o/p transitions.
- Also the positive feedback, because of its regenerative action, will make  $V_0$  switch faster between  $+V_{sat}$  and  $-V_{sat}$ .
- Resistance  $R_{comp} = R_1 \parallel R_2$  is used to minimize the offset problems.
- The comparator with positive feedback is said to exhibit hysteresis, a dead band condition. (i.e) when the input of the comparator exceeds  $V_{ut}$  its output switches from  $+V_{sat}$  to  $-V_{sat}$  and reverts to its original state,  $+V_{sat}$  when the input goes below  $V_{LT}$ . The hysteresis voltage is equal to the difference between  $V_{UT}$  and  $V_{LT}$ . Therefore  $V_H = V_{UT} - V_{LT}$ .



Fig(b,c). Transfer characteristics of  $V_i$  increasing & decreasing  
 d) composite i/p –o/p curve