

## 2.2 ANALYSIS OF CONTINUOUS BEAMS IN SLOPE DEFLECTION METHOD.

### 2.2.1 NUMERICAL EXAMPLES ON( CONTINUOUS BEAMS ):

#### PROBLEM NO:01

Analysis the continuous beam shown in fig.2.8, Calculate the support moments using slope deflection method. Draw the SF and BM diagrams.

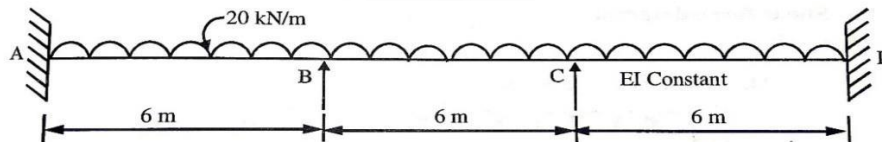


Fig. 2.8

Solutions:

- **Fixed End Moments:**

$$MF_{AB} = MF_{BC} = MF_{CD} = -\frac{Wl^2}{12} = -\frac{20 \times 6^2}{12} = -60 \text{ kNm}$$

$$MF_{BA} = MF_{CB} = MF_{DC} = \frac{Wl^2}{12} = \frac{20 \times 6^2}{12} = 60 \text{ kNm}$$

- **Slope Deflection Equations:**

The structure is symmetrical. So is the load. There is no sinking of supports. Hence the following conditions prevail.

- $\theta_A = \theta_D = 0$
- $\delta = 0$  for all spans
- $\theta_B = \theta_C$

Hence there is only one unknown displacement, namely  $\theta_B$ . For span AB, the general slope deflection equation is

$$M_{AB} = MF_{AB} + \frac{2EI}{6}(2\theta_A + \theta_B + 3\delta/l)$$

$$M_{AB} = -60 + \frac{2EI}{6}(\theta_B) \text{-----(2.1)}$$

Since  $\theta_A = 0$  and  $\delta = 0$

$$M_{AB} = 60 + \frac{2EI}{6}(\theta_B) \text{----- (2.2)}$$

No other slope deflection equation is needed.

Since  $\theta_B$  is the only unknown.

For span BC,

$$M_{BC} = M_{FBC} + 2EI/6(2\theta_B + \theta_C + 3\delta/l)$$

$$M_{BC} = -60 + 2EI/6(3\theta_B) \text{ ----- (2.3)}$$

- Joint Equilibrium Equations:**

$$M_{AB} + M_{BC} = 0$$

$$60 + 2EI\theta_B/3 - 60 + EI\theta_B = 0$$

$$\text{Hence, } \theta_B = 0$$

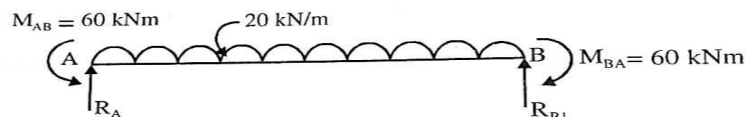
- Final Moments:**

$$M_{AB} = M_{BC} = M_{CD} = -60 \text{ kNm}$$

$$M_{BA} = M_{CB} = M_{DC} = 60 \text{ kNm}$$

- Shear Force Diagram:**

**Span AB:**



Taking moments about A, on the free body diagram of span AB,

$$-R_{B1} \times 6 - M_{AB} + M_{BA} + w l^2/2 = 0$$

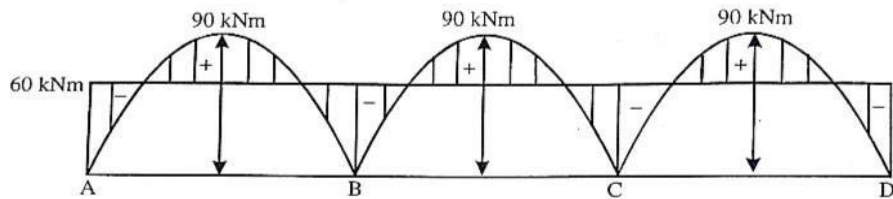
$$-R_{B1} \times 6 - 60 + 60 + 20 \times 6^2/2 = 0$$

$$R_{B1} = 60 \text{ kN ; } R_A = 60 \text{ kN}$$

Similarly in span BC,  $R_{B2} = R_{C1} = 60$

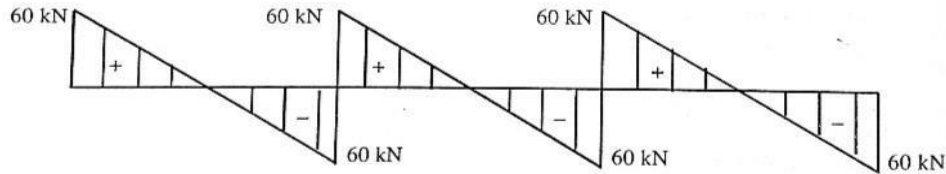
$$R_B = R_{B1} + R_{B2} = 120 \text{ kN}$$

- BMD and SFD:**



Bending moment diagram

$$\text{Simply supported span bending moment} = \frac{wl^2}{8} = \frac{20 \times 6^2}{8} = 90 \text{ kNm}$$



Shear force diagram

## PROBLEM NO:02

Analysis the continuous beam shown in fig.2.10, Calculate the support moments using slope deflection method. Support B sinks by 10mm. Take  $E = 2 \times 10^5 \text{ N/mm}^2$ ,  $I = 16 \times 10^7 \text{ mm}^4$ . Sketch the SF and BM diagrams.

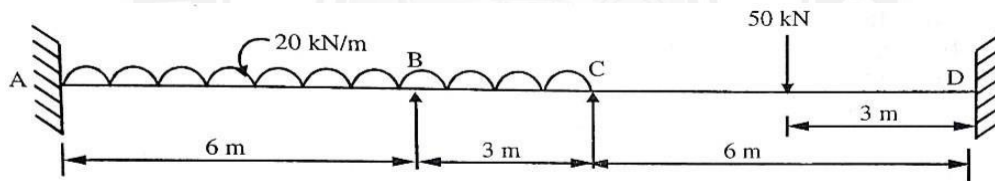


Fig. 2.10

### Solution:

- Fixed End Moments:**

$$MF_{AB} = -Wl^2/12 = -20 \times 6^2/12 = -60 \text{ kNm};$$

$$MF_{BA} = Wl^2/12 = 20 \times 6^2/12 = 60 \text{ kNm};$$

$$MF_{BC} = -Wl^2/12 = -20 \times 3^2/12 = -15 \text{ kNm};$$

$$MF_{CB} = Wl^2/12 = 20 \times 3^2/12 = 15 \text{ kNm};$$

$$MF_{CD} = -Wl/8 = -50 \times 6/8 = -37.5 \text{ kNm};$$

$$MF_{DC} = Wl/8 = 50 \times 6/8 = 37.5 \text{ kNm};$$

- Slope Deflection Equations:**

$$M_{AB} = MF_{AB} + 2EI/6(2\theta_A + \theta_B + 3\delta/l)$$

$$= -60 + EI/3(0 + \theta_B - 1/200) \quad \text{--- (1)}$$

$$M_{BA} = MF_{BA} + 2EI/6(2\theta_B + \theta_A + 3\delta/l)$$

$$= 60 + EI/3(2\theta_B - 3 \times 10/6000) \quad \text{--- (2)}$$

$$MBC = MFBC + 2EI/3(2\theta_B + \theta_C + 3\delta/l)$$

$$= -15 + 2EI/3(2\theta_B + \theta_C + 1/100) \quad \text{--- (3)}$$

$$MCB = MFBC + 2EI/3(2\theta_C + \theta_B + 3\delta/l)$$

$$= 15 + 2EI/3(2\theta_C + \theta_B + 1/100) \quad \text{--- (4)}$$

$$MCD = MFCD + 2EI/6(2\theta_C + \theta_D + 3\delta/l)$$

$$= -37.5 + EI/3(2\theta_C) \quad \text{--- (5)}$$

$$MDC = MFDC + 2EI/6(2\theta_D + \theta_C + 3\delta/l)$$

$$= 37.5 + EI/3(\theta_C) \quad \text{--- (6)}$$

• **Joint Equilibrium Equations:**

Joint B:

$$MBA + MBC = 0$$

$$EI/3(6\theta_B + 2\theta_C + 3/200) = -135 \quad \text{--- (7)}$$

Joint C:

$$MCB + MCD = 0$$

$$EI(\theta_B + 3\theta_C + 1/100) = 33.75 \quad \text{--- (8)}$$

Equating (7 & 8); we get

$$\theta_C = -1/464; \quad \theta_B = -1/402$$

• **Final Moments:**

$$MAB = -139.843 \text{ kNm};$$

$$MBA = -46.354 \text{ kNm};$$

$$MBC = 46.3 \text{ kNm};$$

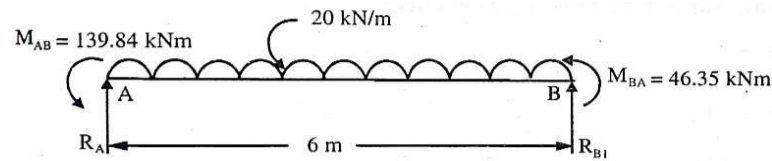
$$MCB = 83.35 \text{ kNm};$$

$$MCD = -83.477 \text{ kNm};$$

$$MDC = 14.51 \text{ kNm};$$

• **To Draw S.F.D:**

Span AB:

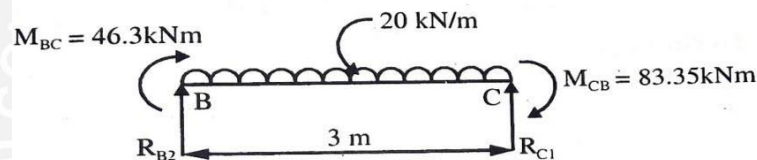


Taking moments about A.

$$20 \times 6^2/2 - 46.35 - 139.84 - R_{B1}(6) = 0; R_{B1} = 28.97 \text{ KN}$$

$$R_A = 20 \times 6 - 28.97; R_A = 91.03 \text{ KN}$$

Span BC:

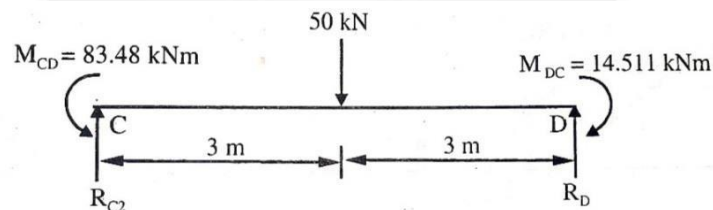


Taking moments about B.

$$20 \times 3^2/2 + 83.35 + 46.3 - R_{C1}(3) = 0; R_{C1} = 73.22 \text{ KN}$$

$$R_{B2} = 20 \times 3 - 73.22; R_{B2} = -13.21 \text{ KN}$$

Span CD:



Taking moments about C.

$$14.511 + 50(3) - 83.48 - R_D(6) = 0;$$

$$R_D = 13.5 \text{ KN}; R_{C2} = 36.5 \text{ KN}$$

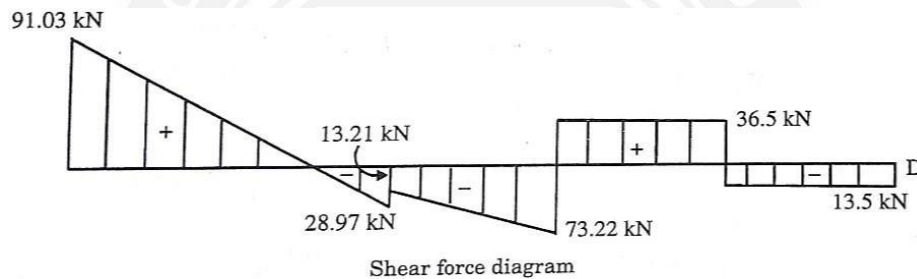
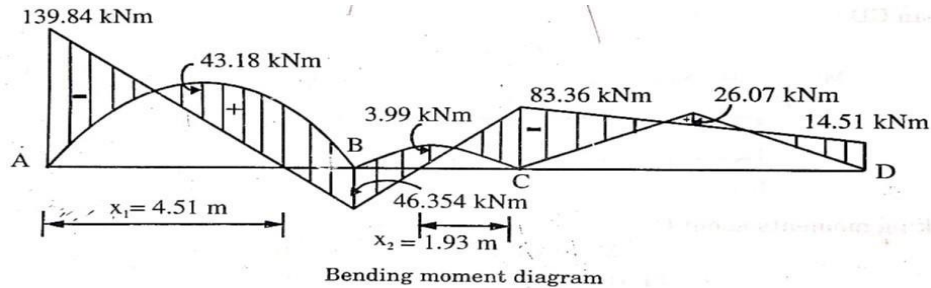
- **Free BMD:**

$$M_{AB} = Wl^2/8 = 20 \times 6^2/8 = 90 \text{ kNm}$$

$$M_{BC} = Wl^2/8 = 20 \times 3^2/8 = 22.5 \text{ kNm}$$

$$M_{CD} = Wl/4 = 50 \times 6/4 = 75 \text{ kNm}$$

- **BMD and SFD:**



### PROBLEM NO:03

Analysis the continuous beam shown in fig.2.3, Calculate the support moments using slope deflection method. Sketch the BM diagrams.

$$2I_{AB} = I_{BC} = 2I_{CD} = 2I$$

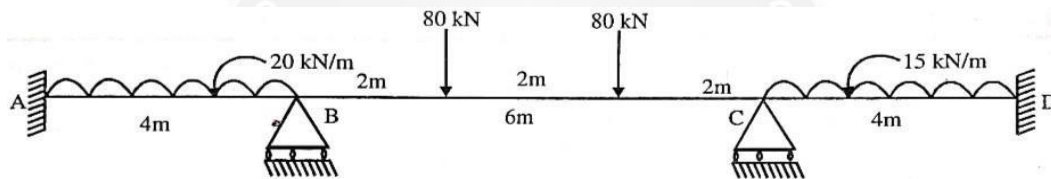


Fig. 2.3

$$I_{AB} = I_{CD} = I, I_{BC} = 2I, \theta_A = \theta_D = 0 \text{ (A and D are fixed)}$$

Solution:

- **Fixed End Moments:**

$$M_{FAB} = -Wl^2/12 = -20 \times 4^2/12 = -26.67 \text{ kNm};$$

$$M_{FBA} = Wl^2/12 = 20 \times 4^2/12 = 26.67 \text{ kNm};$$

$$MFBC = -Wa(a + c)/6 = - 80(4 + 2)/6 = - 106.67 \text{ kNm};$$

$$MFCB = Wa(a + c)/6 = 80(4 + 2)/6 = 106.67 \text{ kNm};$$

$$MFCD = -Wl^2/12 = - 15 \times 4^2/12 = - 20 \text{ kNm};$$

$$MFDC = Wl^2/12 = 15 \times 4^2/12 = 20 \text{ kNm};$$

• **Slope Deflection Equations:**

$$\begin{aligned} MAB &= MFAB + 2EI/6(2\theta_A + \theta_B + 3\delta/l) \\ &= - 26.67 + 0.5EI\theta_B \end{aligned} \quad \text{--- (1)}$$

$$\begin{aligned} MBA &= MFBA + 2EI/6(2\theta_B + \theta_A + 3\delta/l) \\ &= 26.67 + 0.5EI\theta_B \end{aligned} \quad \text{--- (2)}$$

$$\begin{aligned} MBC &= MFBC + 2EI/3(2\theta_B + \theta_C + 3\delta/l) \\ &= - 106.67 + EI(1.332\theta_B + 0.666\theta_C) \end{aligned} \quad \text{--- (3)}$$

$$\begin{aligned} MCB &= MFCB + 2EI/3(2\theta_C + \theta_B + 3\delta/l) \\ &= 106.67 + EI(1.332\theta_C + 0.666\theta_B) \end{aligned} \quad \text{--- (4)}$$

$$\begin{aligned} MCD &= MFCD + 2EI/6(2\theta_C + \theta_D + 3\delta/l) \\ &= - 20 + EI\theta_C \end{aligned} \quad \text{--- (5)}$$

$$\begin{aligned} MDC &= MFDC + 2EI/6(2\theta_D + \theta_C + 3\delta/l) \\ &= 20 + EI(0.5\theta_C) \end{aligned} \quad \text{--- (6)}$$

• **Joint Equilibrium Equations:**

Joint B:

$$\begin{aligned} MBA + MBC &= 0 \\ 2.333\theta_B + 0.666\theta_C &= 80/EI \end{aligned} \quad \text{--- (7)}$$

Joint C:

$$\begin{aligned} MCB + MCD &= 0 \\ 0.666\theta_B + 2.333\theta_C &= 86.67/EI \end{aligned} \quad \text{--- (8)}$$

Equating (7 & 8); we get

$$\theta_C = - 51.11/EI; \quad \theta_B = 48.88/EI;$$

• **Final Moments:**

$$MAB = - 2.23 \text{ kNm};$$

$$MBA = 75.55 \text{ kNm};$$

$$MBC = - 75.55 \text{ kNm};$$

$$MCB = 71.09 \text{ kNm};$$

$$MCD = - 71.09 \text{ kNm};$$

$$MDC = - 5.56 \text{ kNm};$$

- BMD:**

