

## PRINCIPAL PLANES AND PRINCIPAL STRESSES

The planes, which have no shear stress are known as principal planes. Hence principal planes are the planes of zero shear stress. These planes carry only normal stresses.

The normal stresses acting on a principal plane, are known as principal stresses.

## METHODS FOR DETERMINING STRESSES ON OBLIQUE SECTION

The stresses on oblique section are determined by the following methods:

1. Analytical method and 2. Graphical method.

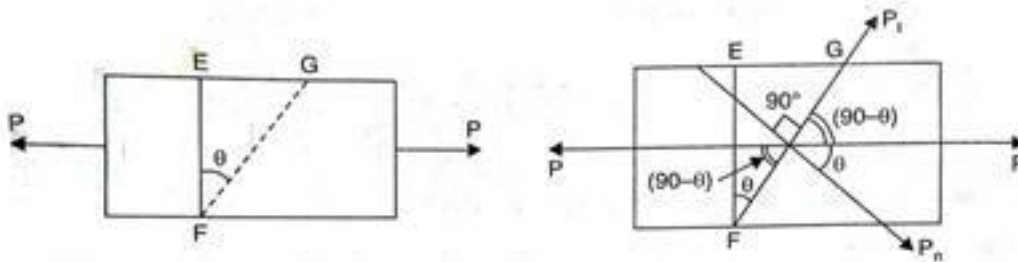
### 1.5.2 ANALYTICAL METHOD FOR DETERMINING STRESSES ON OBLIQUE SECTION

The following two cases will be considered for determining stresses on oblique plane.

1. A member subjected to a direct stress in one plane.
2. The member is subjected to like direct stresses in two mutually perpendicular directions.

#### 1.5.2.1 A Member subjected to a Direct stress in one plane.

Figure shows a rectangular member of uniform cross sectional area  $A$  and of unit thickness



Let  $P$  = Axial force acting on the member

$A$  = Area of cross section, which is perpendicular to the line of action of the force  $P$ .

The stress acting along  $X$  axis,  $\sigma = \frac{P}{A}$

Hence, the member is subjected to a stress along  $X$  axis.

Consider a cross section  $EF$  which is perpendicular to the line of action of the force  $P$ .

Then the area of section,  $EF = EF \times 1 = A$

The stress on the section  $EF$  is given by

$$\sigma = \frac{\text{Force}}{\text{Area of } EF} = \frac{P}{A}$$

The stress on the section  $EF$  is entirely normal stress. There is no shear stress (or tangential stress) on the section  $EF$ .

Now consider a section  $FG$  at an angle  $\theta$  with the normal cross section  $EF$  as shown in Figure

$$\text{Area of FG} = FG \times 1 = FG$$

$$= \frac{EF}{\cos\theta} \times 1 \quad (\text{since In } \triangle EFG, \theta = \frac{EF}{FG} \therefore FG = \frac{E}{\cos\theta})$$

$$= \frac{A}{\cos\theta}$$

$$\therefore \text{Stress on the section, FG} = \frac{\text{Force}}{\text{Area of section FG}} = \frac{P}{\frac{A}{\cos\theta}} = \frac{P}{A} \cos\theta$$

$$= \sigma \cos\theta \quad (\text{since } \sigma = \frac{P}{A}) \quad \dots(i)$$

This stress on the section FG, is parallel to the axis of the member (i.e., this stress is along X axis). This stress may be resolved in two components. One component will be normal to the section FG whereas the second component will be along the section FG (i.e., tangential stress on the section FG). The normal stress and tangential stress (i.e., shear stress) on the section FG are obtained as given below. (Refer above Fig.)

Let  $P_n$  = The component of the force P, normal to section FG =  $P \cos\theta$

$P_t$  = The component of force P, along the section FG (or tangential to the surface FG)  
=  $P \sin\theta$

$\sigma_n$  = Normal stress across the section FG

$\sigma_t$  = Tangential stress (i.e., shear stress) across the section FG.

$$\text{Normal stress } \sigma_n = \frac{\text{Force normal to section FG}}{\text{Area of section FG}}$$

$$= \frac{P_n}{\frac{A}{\cos\theta}} \quad (\text{since } P_n = P \cos\theta)$$

$$= \frac{P \cos\theta}{\frac{A}{\cos\theta}}$$

$$= \frac{P \cos\theta \cdot \cos\theta}{A} = \frac{P \cos^2\theta}{A}$$

$$= \sigma \cos^2\theta \quad \dots(ii) \quad \text{Tangential stress(or)}$$

Shear stress,

$$\sigma_t = \frac{\text{Tangential force across section FG}}{\text{Area of section FG}}$$

$$= \frac{P_t}{\frac{A}{\cos\theta}} \quad (\text{since } P_t = P \sin\theta)$$

$$= \frac{P \sin\theta}{\frac{A}{\cos\theta}}$$

$$= \frac{P \sin\theta \cdot \cos\theta}{A} = \sigma \sin\theta \cdot \cos\theta$$

$$= \frac{\sigma \sin 2\theta}{2} \quad \dots(iii)$$

$$[\because \text{since } \sin 2\theta = 2\sin\theta\cos\theta \quad \sin\theta\cos\theta = \sin 2\theta/2]$$

From equation (ii) it is seen that the normal stress ( $\sigma_n$ ) on the section FG will be maximum when  $\cos^2\theta$  or  $\cos\theta$  is maximum. And  $\cos\theta$  will be maximum when  $\theta=0^\circ$  as  $\cos 0=1$ . But when  $\theta=0^\circ$ , the section FG will coincide with section EF. But the section EF is normal to the line of action of the loading. This means the plane normal to the axis of loading. This means the plane normal to the axis of loading will carry the maximum normal stress.

$$\therefore \text{Maximum normal stress, } = \sigma\cos^2\theta = \sigma\cos^2 0 = \sigma \quad \dots(\text{iv})$$

From equation (iii), it is observed that the tangential stress (i.e., shear stress) across the section FG will be maximum when  $\sin 2\theta=1$  or  $2\theta=90^\circ$  or  $270^\circ$

$$\text{or } \theta = 45^\circ \text{ or } 135^\circ$$

This means the shear stress will be maximum on two planes inclined at  $45^\circ$  and  $135^\circ$  to the normal section EF as shown in fig.

$$\therefore \text{Max. value of shear stress } = \frac{\sigma\sin 2\theta}{2} = \frac{\sigma\sin 90^\circ}{2} = \frac{\sigma}{2} \quad \dots(\text{v})$$

From equations (iv) and (v) it is seen that maximum normal stress is equal to  $\sigma$  Whereas the maximum shear stress is equal to  $\frac{\sigma}{2}$  or equal to half the value of greatest normal stress.

**A member subjected to like Direct stresses in two mutually perpendicular Directions.**

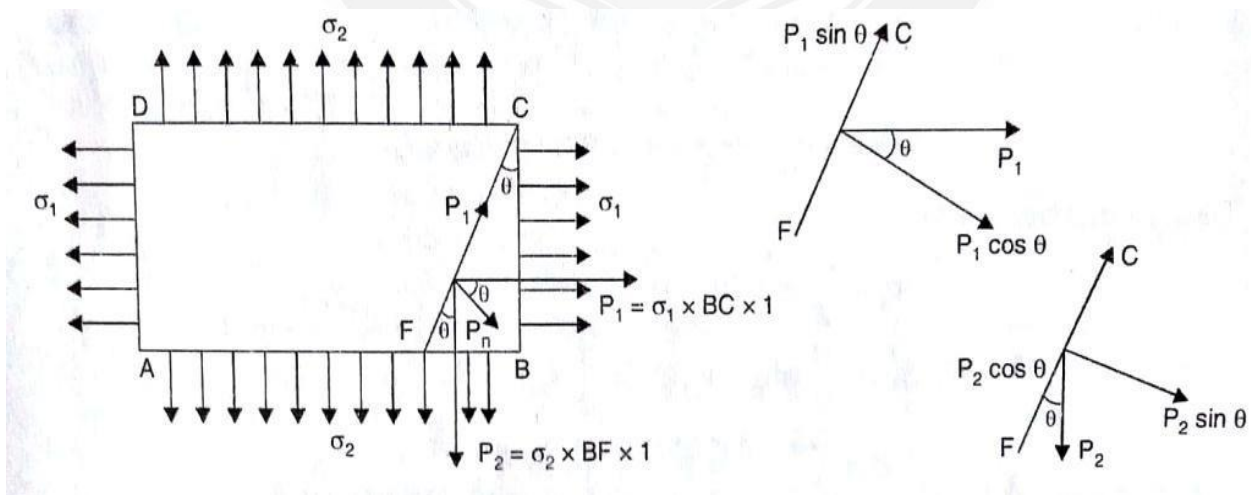


Fig. shows a rectangular bar ABCD of uniform cross sectional area A and of uniform thickness. The bar is subjected to two direct tensile stresses (or two principal tensile stresses) as shown in Fig

Let FC be the oblique section on which stresses are to be calculated. This can be done by converting the stresses  $\sigma_1$  (acting along on face BC) and  $\sigma_2$  (acting on face AB) into

equivalent forces. Then these forces will be resolved along the incline plane FC and perpendicular to FC. Consider the forces acting on wedge FBC.

Let  $\theta$  = Angle made by oblique section FC with normal cross section BC

$\sigma_1$  = Major tensile stress on face AD and BC

$\sigma_2$  = Minor tensile stress on face AB and CD

$P_1$  = Tensile force on face BC

$P_2$  = Tensile force on face FB.

The tensile force on face BC,

$$P_1 = \sigma_1 \times \text{Area of face BC} = \sigma_1 \times BC \times 1$$

The tensile force on face FB,

$$P_2 = \sigma_2 \times \text{Area of face FB} = \sigma_2 \times FB \times 1$$

The tensile forces  $P_1$  and  $P_2$  are also acting on the oblique section FC. The force  $P_1$  is acting in the axial direction, whereas the force  $P_2$  is acting downwards as shown in Fig. Two forces  $P_1$  and  $P_2$  each can be resolved into two components i.e., one normal to the plane FC and the other along the plane FC. The components of  $P_1$  and  $P_1 \cos \theta$  normal to the plane FC and  $P_1 \sin \theta$  along the plane in the upward direction. The components of  $P_2$  and  $P_2 \sin \theta$  normal to the plane FC and  $P_2 \cos \theta$  along the plane in the downward direction.

$$\begin{aligned} \text{Let } P_n &= \text{Total force normal to section FC} \\ &= \text{Component of force } P_1 \text{ normal to the section FC} + \text{Component of force } P_2 \\ &\text{normal to the section FC} \\ &= P_1 \cos \theta + P_2 \sin \theta \\ &= \sigma_1 \times BC \times \cos \theta + \sigma_2 \times FB \times \sin \theta \\ &\quad (\text{since } P_1 = \sigma_1 \times BC, P_2 = \sigma_2 \times FB) \end{aligned}$$

$$\begin{aligned} P_t &= \text{Total force along the section FC} \\ &= \text{Component of force } P_1 \text{ along the section FC} + \text{Component of force } P_2 \\ &\text{along the section FC} \end{aligned}$$

$$= P_1 \sin \theta - P_2 \cos \theta \quad (\text{-ve sign is taken due to opposite direction})$$

$$= \sigma_1 \times BC \times \sin \theta - \sigma_2 \times FB \times \cos \theta \quad (\because P_1 = \sigma_1 \times BC, P_2 = \sigma_2 \times FB)$$

$\sigma_n$  = Normal stress across the section FC

$$\begin{aligned} &= \frac{\text{Total force normal to the section FC}}{\text{Area of section FC}} \\ &= \frac{P_n}{FC \times 1} = \frac{1 \times BC \times \cos \theta + \sigma_2 \times BF \times \sin \theta}{FC} \end{aligned}$$

$$\begin{aligned}
 &= \sigma_1 \times \frac{BC}{FC} \times \cos\theta + \sigma_2 \times \frac{BF}{FC} \times \sin\theta \\
 &= \sigma_1 \times \cos\theta \times \cos\theta + \sigma_2 \times \sin\theta \times \sin\theta \\
 &= \sigma_1 \times \cos^2\theta + \sigma_2 \times \sin^2\theta \\
 &= \sigma_1 \times \frac{1 + \cos 2\theta}{2} + \sigma_2 \times \frac{1 - \cos 2\theta}{2} \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta
 \end{aligned}$$

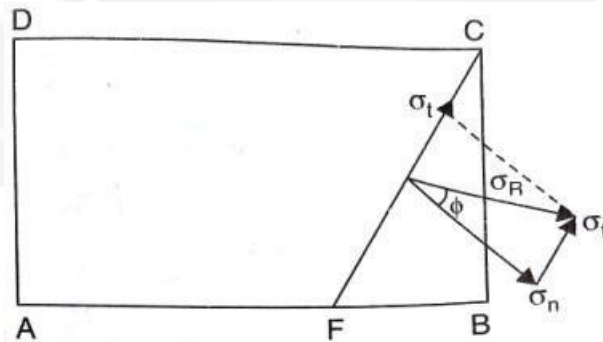
$\sigma_t$  = Tangential stress (or shear stress) along section FC

$$\begin{aligned}
 &= \frac{\text{Total force along the section FC}}{\text{Area of section FC}} \\
 &= \frac{P_t}{FC \times 1} = \frac{\sigma_1 \times BC \times \sin\theta - \sigma_2 \times BF \times \cos\theta}{FC} \\
 &= \sigma_1 \times \frac{BC}{FC} \times \sin\theta - \sigma_2 \times \frac{BF}{FC} \times \cos\theta \\
 &= \sigma_1 \times \cos\theta \times \sin\theta - \sigma_2 \times \sin\theta \times \cos\theta \\
 &= (\sigma_1 - \sigma_2) \cos\theta \times \sin\theta \\
 &= \frac{(\sigma_1 - \sigma_2)}{2} \times 2 \cos\theta \times \sin\theta \\
 &= \frac{(\sigma_1 - \sigma_2)}{2} \sin 2\theta
 \end{aligned}$$

The resultant stress on the section FC will be given as

$$\sigma_R = \sqrt{\sigma_n^2 + \sigma_t^2}$$

**Obliquity.** The angle made by the resultant stress with the normal of the oblique plane, is known as obliquity as shown in fig. Mathematically, it is denoted by,  $\tan\phi = \frac{\sigma_t}{\sigma_n}$



**Maximum Shear stress.** The shear stress is given by  $\sigma_t = \frac{(\sigma_1 - \sigma_2)}{2} \sin 2\theta$ . The shear stress

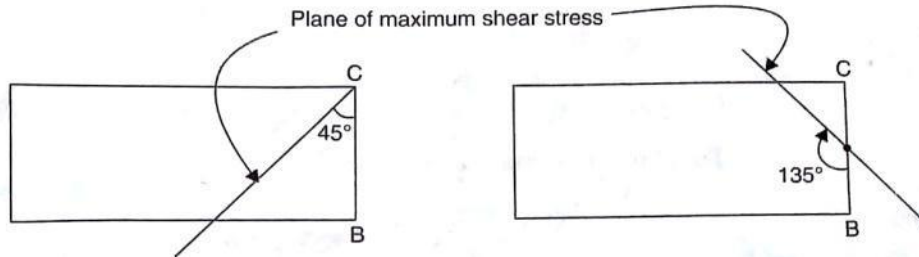
will be maximum when

$$\sin 2\theta = 1 \text{ or } 2\theta = 90^\circ \text{ or } 270^\circ$$

$$\therefore \theta = 45^\circ \text{ or } 135^\circ$$

And maximum shear stress  $(\sigma_t)_{\max} = \frac{(\sigma_1 - \sigma_2)}{2}$

The planes of maximum shear stress are obtained by making an angle of  $45^\circ$  and  $135^\circ$  with the plane BC (at any point on the plane BC) in such a way that the planes of maximum shear stress lie within the material as shown in Fig.



### Principal Planes

Principal planes are the planes on which shear stress is zero. To locate the position of principal planes, the shear stress should be equated to zero.

$\therefore$  For principal planes,  $\frac{(\sigma_1 - \sigma_2)}{2} \sin 2\theta = 0$

Or  $\sin 2\theta = 0$  (since  $(\sigma_1 - \sigma_2)$  cannot be 0)

Or  $2\theta = 0$  or  $180^\circ$

Or  $\theta = 0$  or  $90^\circ$

When  $\theta = 0$ ,

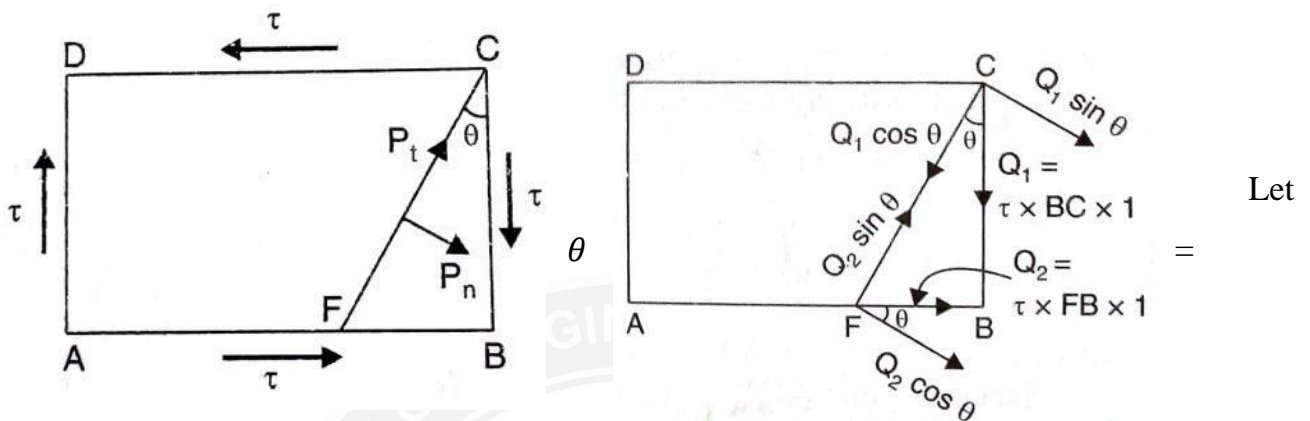
$$\begin{aligned} \sigma_n &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta \\ &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 0 \\ &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \\ &= \sigma_1 \end{aligned}$$

When  $\theta = 90^\circ$ ,

$$\begin{aligned} \sigma_n &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos(2 \times 90^\circ) \\ &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 180^\circ \\ &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \times -1 \\ &= \sigma_2 \end{aligned}$$

**A member subjected to simple shear stress.**

Fig. shows a rectangular bar ABCD of uniform cross sectional area A and of unit thickness. The bar is subjected to a simple shear stress ( $\tau$ ) across the faces BC and AD. Let FC be the oblique section on which normal and tangential stress are to be calculated.



Angle made by oblique section FC with normal cross section BC,

$\tau$  = Shear stress across faces BC and AD.

It has already been proved that a shear stress is always accompanied by an equal shear stress at right angles to it. Hence the faces AB and CD will also be subjected to a shear stress  $\tau$  as shown in above Fig. Now these stress will be converted in to equal forces. Then these forces will be resolved along the inclined surface and normal to the inclined surface. Consider the forces acting on the wedge FBC of fig.

Let  $Q_1$  = shear force on face BC  
 = Shear stress  $\times$  Area of face BC  
 =  $\tau \times BC \times 1$  (Since Area of BC = BC  $\times$  1)  
 =  $\tau \times BC$

$Q_2$  = shear force on face FB  
 = Shear stress  $\times$  Area of face FB  
 =  $\tau \times FB \times 1$  (Since Area of FB = FB  $\times$  1)  
 =  $\tau \times FB$

$P_n$  = Total normal force on section FC

$P_t$  = Total tangential force on section FC

The force  $Q_1$  is acting along face CB as shown in Fig. This force is resolved into two components. i.e.,  $Q_1 \cos \theta$  and  $Q_1 \sin \theta$  along the plane CF and normal to the plane CF respectively.

The force  $Q_2$  is acting along face FB as shown in Fig. This force is resolved into two components. i.e.,  $Q_2 \sin \theta$  and  $Q_2 \cos \theta$  along the plane FC and normal to the plane FC respectively.

∴ Total normal force of section FC,

$$\begin{aligned} P_n &= Q_1 \sin \theta + Q_2 \cos \theta \\ &= r \times BC \sin \theta + r \times FB \cos \theta \quad (\text{since } Q_1 = r \times BC \text{ and } Q_2 = r \times FB) \end{aligned}$$

And total tangential force on section FC.

$$\begin{aligned} P_t &= Q_2 \sin \theta - Q_1 \cos \theta \quad (\text{-ve sign is taken due to opposite direction}) \\ &= r \times FB \sin \theta - r \times BC \cos \theta \end{aligned}$$

Let  $\sigma_n$  = Normal stress on section FC

$\sigma_t$  = Tangential stress on section FC

$$\sigma_n = \frac{\text{Total normal force on section FC}}{\text{Area of section FC}}$$

$$= \frac{P_n}{FC \times 1}$$

$$= \frac{r \times BC \sin \theta + r \times FB \cos \theta}{FC \times 1}$$

$$= r \frac{BC}{FC} \sin \theta + r \frac{FB}{FC} \cos \theta$$

$$= r \cos \theta \sin \theta + r \sin \theta \cos \theta$$

$$= 2 r \cos \theta \sin \theta$$

$$= r \sin 2\theta$$

$$\sigma_t = \frac{\text{Total tangential force on section FC}}{\text{Area of section FC}}$$

$$= \frac{P_t}{FC \times 1}$$

$$= \frac{c \times FB \sin \theta - c \times BC \cos \theta}{FC \times 1}$$

$$= r \frac{FB}{FC} \sin \theta - r \frac{BC}{FC} \cos \theta$$

$$= r \sin \theta \sin \theta - r \cos \theta \cos \theta$$

$$= r \sin^2 \theta - r \cos^2 \theta$$

$$= -r (\cos^2 \theta - \sin^2 \theta)$$

$$= -r \cos 2\theta$$

-ve sign shows that  $\sigma_t$  will be acting downwards on the plane CF.

**A member subjected to Direct stresses in two mutually perpendicular Directions Accompanied by a simple shear stress.**



Above fig. shows a rectangular bar ABCD of uniform cross sectional area  $A$  and of unit thickness. The bar is subjected to :

- (i) tensile stress  $\sigma_1$  on the face BC and AD
- (ii) tensile stress  $\sigma_2$  on the face AB and CD
- (iii) a simple shear stress  $r$  on face BC and AD.

The forces acting on the wedge FBC are:

$$\begin{aligned} P_1 &= \text{Tensile force on face BC due to tensile stress } \sigma_1 \\ &= \sigma_1 \times \text{Area of BC} \\ &= \sigma_1 \times BC \times 1 \\ &= \sigma_1 \times BC \end{aligned}$$

$$\begin{aligned} P_2 &= \text{Tensile force on face FB due to tensile stress } \sigma_2 \\ &= \sigma_2 \times \text{Area of FB} \\ &= \sigma_2 \times FB \times 1 \\ &= \sigma_2 \times FB \end{aligned}$$

$$\begin{aligned} Q_1 &= \text{Shear force on the face BC due to shear stress } r \\ &= r \times \text{Area of BC} \\ &= r \times BC \times 1 \\ &= r \times BC \end{aligned}$$

$$\begin{aligned} Q_2 &= \text{Shear force on the face FB due to shear stress } r \\ &= r \times \text{Area of FB} \\ &= r \times FB \times 1 \\ &= r \times FB \end{aligned}$$

Resolving the above four forces (i.e.,  $P_1, P_2, Q_1$ , and  $Q_2$ ) normal to the oblique section FC, we get

Total normal force,

$$P_n = P_1 \cos \theta + P_2 \sin \theta + Q_1 \sin \theta + Q_2 \cos \theta$$

Substituting the values of  $P_1, P_2, Q_1$ , and  $Q_2$ , we get

$$P_n = \sigma_1 \cdot BC \cdot \cos \theta + \sigma_2 \cdot FB \cdot \sin \theta + r \cdot BC \cdot \sin \theta + r \cdot FB \cdot \cos \theta$$

Similarly, the total tangential force ( $P_t$ ) is obtained by resolving  $P_1, P_2, Q_1$  and  $Q_2$  along the oblique section FC

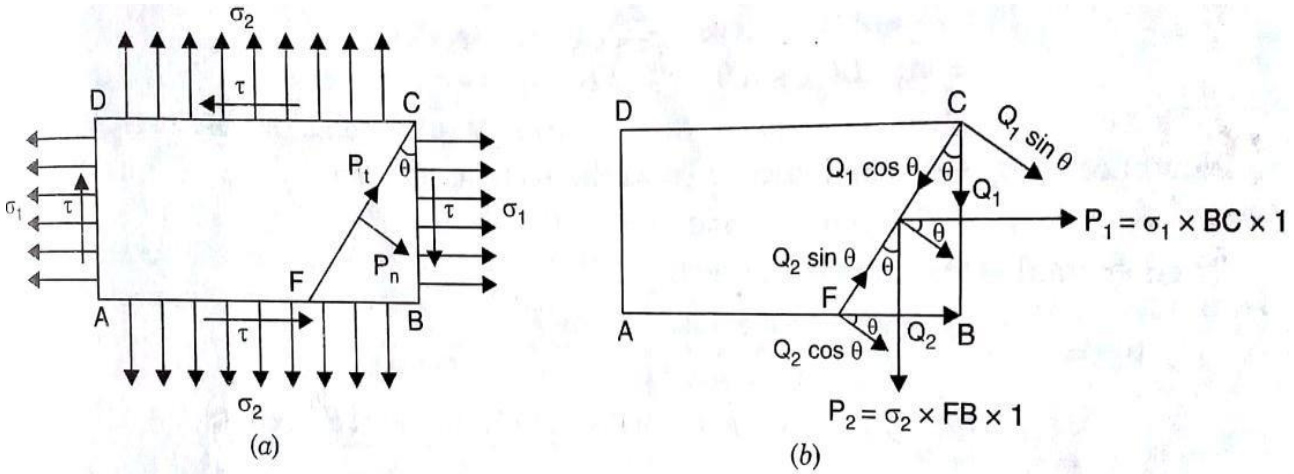
∴ Total tangential force,

$$P_t = P_1 \sin \theta - P_2 \cos \theta - Q_1 \cos \theta + Q_2 \sin \theta$$

$$= \sigma_1 \cdot BC \sin\theta - \sigma_2 \cdot FB \cos\theta - r \cdot BC \cos\theta + r \cdot FB \sin\theta$$

Now, Let  $\sigma_n$  = Normal stress across the section FC, and

$\sigma_t$  = Tangential stress across the section FC,



$$\begin{aligned} \sigma_n &= \frac{\text{Total normal force across section FC}}{\text{Area of section FC}} \\ &= \frac{P_n}{FC \times 1} \\ &= \frac{\sigma_1 BC \cdot \cos\theta + \sigma_2 FB \cdot \sin\theta + \tau BC \cdot \sin\theta + \tau FB \cdot \cos\theta}{FC \times 1} \\ &= \sigma_1 \frac{BC \cdot \cos\theta}{FC} + \sigma_2 \frac{FB \cdot \sin\theta}{FC} + r \frac{BC \cdot \sin\theta}{FC} + r \frac{FB \cdot \cos\theta}{FC} \\ &= \sigma_1 \cos\theta \cdot \cos\theta + \sigma_2 \sin\theta \cdot \sin\theta + r \cos\theta \cdot \sin\theta + r \sin\theta \cdot \cos\theta \\ &= \sigma_1 \cos^2\theta + \sigma_2 \sin^2\theta + 2r \cos\theta \cdot \sin\theta \\ &= \sigma_1 \frac{1 + \cos 2\theta}{2} + \sigma_2 \frac{1 - \cos 2\theta}{2} + r \sin 2\theta \\ &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta + r \sin 2\theta \quad \dots(i) \end{aligned}$$

**Tangential stress (i.e., shear stress) across the section FC,**

$$\begin{aligned} \sigma_t &= \frac{\text{Total tangential force across section FC}}{\text{Area of section FC}} \\ &= \frac{P_t}{FC \times 1} \\ &= \frac{\sigma_1 BC \cdot \sin\theta - \sigma_2 FB \cdot \cos\theta - r BC \cdot \cos\theta + r FB \cdot \sin\theta}{FC \times 1} \\ &= \sigma_1 \frac{BC \cdot \sin\theta}{FC} - \sigma_2 \frac{FB \cdot \cos\theta}{FC} - r \frac{BC \cdot \cos\theta}{FC} + r \frac{FB \cdot \sin\theta}{FC} \\ &= \sigma_1 \cos\theta \cdot \sin\theta - \sigma_2 \sin\theta \cdot \cos\theta - r \cos\theta \cdot \cos\theta + r \sin\theta \cdot \sin\theta \end{aligned}$$

$$\begin{aligned}
 &= (\sigma_1 - \sigma_2) \cdot \cos\theta \sin\theta - r \cos^2\theta + r \sin^2\theta \\
 &= \frac{\sigma_1 - \sigma_2}{2} 2 \cos\theta \sin\theta - (\cos^2\theta - \sin^2\theta) \\
 &= \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta - r \cos 2\theta \quad \dots(ii)
 \end{aligned}$$

### Position of principal planes.

The planes on which shear stress (i.e., tangential stress) is zero are known as principal planes. And the stress acting on principal planes are known as principal stresses.

The position of principal planes are obtained by equating the tangential stress to zero

∴ For principal planes,  $\sigma_t = 0$

Or  $\frac{\sigma_1 - \sigma_2}{2} \sin 2\theta - r \cos 2\theta = 0$

Or  $\frac{\sigma_1 - \sigma_2}{2} \sin 2\theta = r \cos 2\theta$

Or  $\sin 2\theta = \frac{r \cos 2\theta}{\frac{\sigma_1 - \sigma_2}{2}}$

Or  $\tan 2\theta = \frac{2r}{\sigma_1 - \sigma_2}$

But the tangent of any angle in a right angled triangle

$$\frac{\text{Height of right angled triangle}}{\text{Base of right angled triangle}} = \frac{2r}{\sigma_1 - \sigma_2}$$

Now diagonal of the right angled triangle

$$\begin{aligned}
 &= \sqrt{(\sigma_1 - \sigma_2)^2 + (2r)^2} \\
 &= \pm \sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}
 \end{aligned}$$

### 1<sup>st</sup> case

$$\text{Diagonal} = \sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}$$

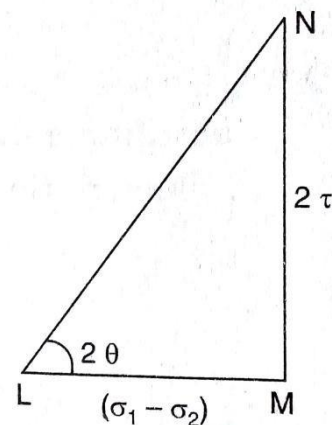
$$\text{Then } \sin 2\theta = \frac{\text{Height}}{\text{Diagonal}} = \frac{2r}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}}$$

$$\text{And } \cos 2\theta = \frac{\text{Base}}{\text{Diagonal}} = \frac{(\sigma_1 - \sigma_2)}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}}$$

The value of major principal stress is obtained by substituting the values of  $\sin 2\theta$  and  $\cos 2\theta$  in equation (i)

∴ Major Principal stress

$$= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta + r \sin 2\theta$$



$$\begin{aligned}
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \frac{(\sigma_1 - \sigma_2)}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} + r \frac{2c}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{1}{2} \frac{(\sigma_1 - \sigma_2)^2}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}} + \frac{2c^2}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{(\sigma_1 - \sigma_2)^2 + 4c^2}{2\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{1}{2} \frac{\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}}{1 - 2} \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \sqrt{\frac{(\sigma_1 - \sigma_2)^2 + 4r^2}{2}} \quad \dots\text{(iii)}
 \end{aligned}$$

2<sup>nd</sup> case

$$\text{Diagonal} = -\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}$$

$$\text{Then } \sin 2\theta = \frac{\text{Height}}{\text{Diagonal}} = \frac{2c}{-\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}}$$

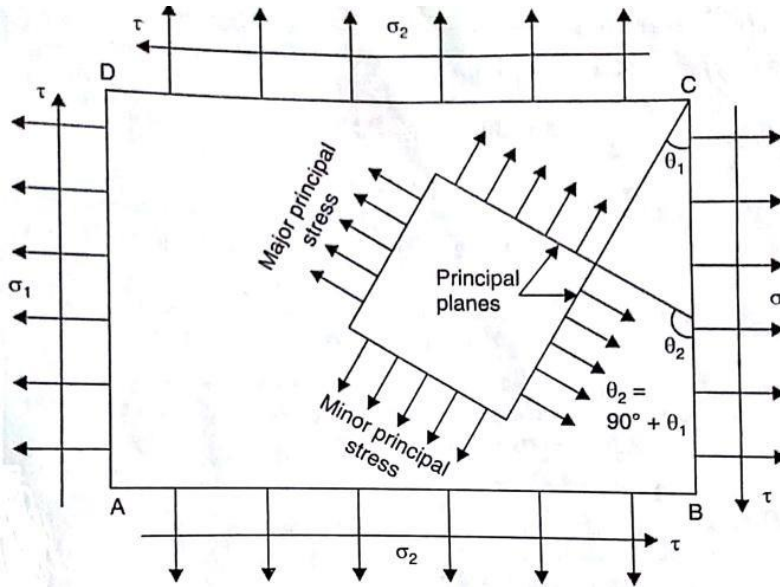
$$\text{And } \cos 2\theta = \frac{\text{Base}}{\text{Diagonal}} = \frac{(\sigma_1 - \sigma_2)}{-\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}}$$

Substituting these values in equation (i), we get minor principal stress

∴ Minor principal stress

$$\begin{aligned}
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta + r \sin 2\theta \\
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \frac{(\sigma_1 - \sigma_2)}{-\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} + r \frac{2c}{-\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} \\
 &= \frac{\sigma_1 + \sigma_2}{2} - \frac{1}{2} \frac{(\sigma_1 - \sigma_2)^2}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} - \frac{2c^2}{\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}} \\
 &= \frac{\sigma_1 + \sigma_2}{2} - \frac{2\sqrt{(\sigma_1 - \sigma_2)^2 + 4c^2}}{2} \\
 &= \frac{\sigma_1 + \sigma_2}{2} - \frac{1}{2} \frac{\sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2}}{1 - 2} \\
 &= \frac{\sigma_1 + \sigma_2}{2} - \sqrt{\frac{(\sigma_1 - \sigma_2)^2 + 4r^2}{2}} \quad \dots\text{(iv)}
 \end{aligned}$$

Equation (iii) gives the maximum principal stress whereas equation (iv) gives the minimum principal stress. The two principal planes are at right angles.



**Maximum shear stress.**

The shear stress will be maximum or minimum when  $\frac{d}{d\theta}(\tau_v) = 0$

$$\frac{d}{d\theta} \left( \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta - r \cos 2\theta \right) = 0$$

$$\frac{\sigma_1 - \sigma_2}{2} (\cos 2\theta) \times 2 - (-\sin 2\theta) \times 2 = 0$$

$$(\sigma_1 - \sigma_2) \cdot \cos 2\theta + 2(\sin 2\theta) = 0$$

$$2(\sin 2\theta) = -(\sigma_1 - \sigma_2) \cdot \cos 2\theta$$

$$= (\sigma_2 - \sigma_1) \cdot \cos 2\theta$$

Or

$$\frac{\sin 2\theta}{\cos 2\theta} = \frac{\sigma_2 - \sigma_1}{2r}$$

Or

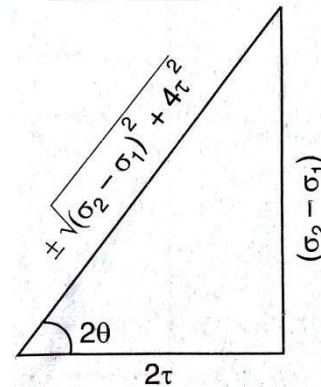
$$\tan 2\theta = \frac{\sigma_2 - \sigma_1}{2c} \dots (v)$$

Equation (v) gives condition for maximum or minimum shear stress.

If  $\tan 2\theta = \frac{\sigma_2 - \sigma_1}{2c}$

Then,  $\sin 2\theta = \frac{\text{height}}{\text{Diagonal}} = \pm \frac{\sigma_2 - \sigma_1}{\sqrt{(\sigma_2 - \sigma_1)^2 + 4c^2}}$

And  $\cos 2\theta = \frac{\text{Base}}{\text{Diagonal}} = \pm \frac{2c}{\sqrt{(\sigma_2 - \sigma_1)^2 + 4c^2}}$

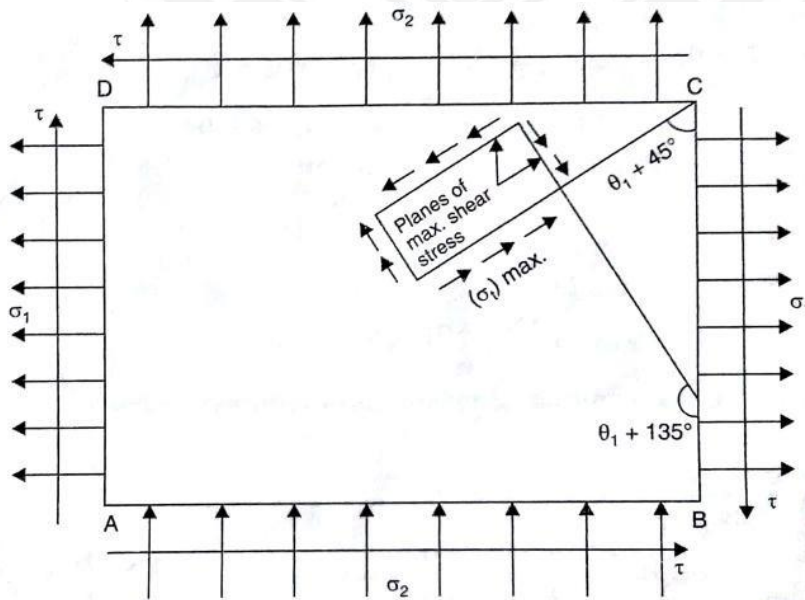


Substituting the values of  $\sin 2\theta$  and  $\cos 2\theta$  in equation (ii), the maximum and minimum shear stresses are obtained.

$$\begin{aligned}
 (\sigma)_{\text{max}} &= \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta - r \cos 2\theta \\
 &= \pm \frac{\sigma_1 - \sigma_2}{2} \times \frac{\sigma_2 - \sigma_1}{\sqrt{(\sigma_2 - \sigma_1)^2 + 4c^2}} \pm r \frac{2c}{\sqrt{(\sigma_2 - \sigma_1)^2 + 4c^2}} \\
 &= \pm \frac{(\sigma_2 - \sigma_1)^2}{2\sqrt{(\sigma_2 - \sigma_1)^2 + 4r^2}} \pm \frac{2r^2}{\sqrt{(\sigma_2 - \sigma_1)^2 + 4r^2}} \\
 &= \pm \frac{(\sigma_2 - \sigma_1)^2 + 4c^2}{2\sqrt{(\sigma_2 - \sigma_1)^2 + 4c^2}} \\
 &= \pm \frac{1}{2} \sqrt{(\sigma_2 - \sigma_1)^2 + (2r)^2} \\
 (\sigma)_{\text{max}} &= \frac{1}{2} \sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2} \\
 &= \frac{1}{2} \sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2} \quad \dots\text{(vi)}
 \end{aligned}$$

The planes on which maximum shear stress is acting, are obtained after finding the two values of  $\theta$  from equation (v). These two values of  $\theta$  will differ by  $90^\circ$ .

The second method of finding the planes of maximum shear stress is to find first principal planes and principal stresses. Let  $\theta_1$  is the angle of principal plane with plane BC of Fig. Then the planes of maximum shear stress will be at  $\theta_1 + 45^\circ$  and  $\theta_1 + 135^\circ$  with plane BC as shown in below Fig.



tensile  
across two  
planes are  
 $60\text{N/mm}^2$ .  
normal,

**Problem.1.21.**The stresses at a point mutually perpendicular  $120\text{N/mm}^2$  and Determine the tangential and

resultant stresses on a plane inclined at  $30^\circ$  to the axis of minor stress

**Given Data**

Major principal stress,  $\sigma_1 = 120\text{N/mm}^2$

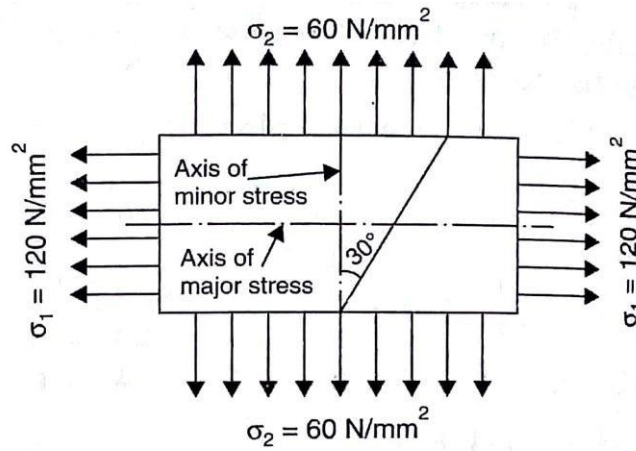
Minor principal stress,  $\sigma_2 = 60\text{N/mm}^2$

Angle of oblique plane with the axis of minor principal stress,

$$\theta = 30^\circ$$

**To find**

The normal, tangential and resultant stresses.



**Normal stress ( $\sigma_n$ )**

$$\begin{aligned}\sigma_n &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta \\ &= \frac{120 + 60}{2} + \frac{120 - 60}{2} \cos 2 \times 30^\circ \\ &= 105 \text{ N/mm}^2\end{aligned}$$

**Tangential stress ( $\sigma_t$ )**

$$\begin{aligned}\sigma_t &= \frac{(\sigma_1 - \sigma_2)}{2} \sin 2\theta \\ &= \frac{120 - 60}{2} \sin 2 \times 30^\circ = 25.98 \text{ N/mm}^2\end{aligned}$$

**Resultant stress ( $\sigma_R$ )**

The resultant stress on the section FC will be given as

$$\begin{aligned}\sigma_R &= \sqrt{\sigma_n^2 + \sigma_t^2} \\ &= \sqrt{105^2 + 25.98^2} = 108.16 \text{ N/mm}^2\end{aligned}$$

**Problem.1.5.4.** The stresses at a point in a bar are  $200 \text{ N/mm}^2$  (tensile) and  $100 \text{ N/mm}^2$  (compressive). Determine the resultant stress in magnitude and direction on a plane inclined at  $60^\circ$  to the axis of major stress. Also determine the maximum intensity of shear stress in the material at the point.

**Given Data**

Major principal stress,  $\sigma_1 = 200\text{N/mm}^2$

Minor principal stress,  $\sigma_2 = -100\text{N/mm}^2$  (-ve sign is due to compressive stress)

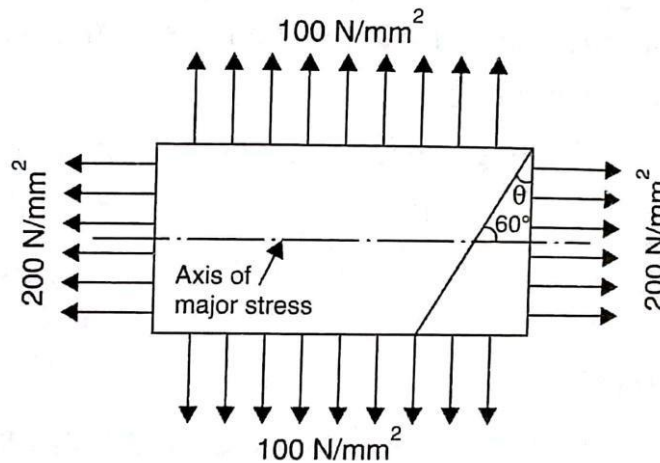
Angle of oblique plane with the axis of minor principal stress,

$$\theta = 90^\circ - 60^\circ = 30^\circ$$

### To find

The Magnitude and direction Resultant stress and maximum intensity of shear stress

### Solution



### Normal stress( $\sigma_n$ )

$$\begin{aligned}\sigma_n &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta \\ &= \frac{200 - 100}{2} + \frac{200 + 100}{2} \cos 2 \times 30^\circ = 125\text{N/mm}^2\end{aligned}$$

### Tangential stress( $\sigma_t$ )

$$\begin{aligned}\sigma_t &= \frac{(\sigma_1 - \sigma_2)}{2} \sin 2\theta \\ &= \frac{200 + 100}{2} \sin 2 \times 30^\circ = 129.9\text{N/mm}^2\end{aligned}$$

### Resultant stress( $\sigma_R$ )

The resultant stress on the section FC will be given as

$$\begin{aligned}\sigma_R &= \sqrt{\sigma_n^2 + \sigma_t^2} \\ &= \sqrt{125^2 + 129.9^2} = 180.27\text{N/mm}^2\end{aligned}$$

### Direction of Resultant stress

$$\tan \theta = \frac{\sigma_t}{\sigma_n} = \frac{129.9}{125} = 1.04$$

$$\theta = \tan^{-1} 1.04 = 46^\circ 6'$$

### Maximum Shear stress



$$\begin{aligned}
 (\sigma_t)_{\max} &= \frac{(200+100)}{2} \\
 &= 150\text{N/mm}^2
 \end{aligned}$$

**Problem.1.5.5.** At a point within a body subjected to two mutually perpendicular directions, the stresses are  $80 \text{ N/mm}^2$  tensile and  $40\text{N/mm}^2$  tensile. Each of the above stresses is accompanied by a shear stress of  $60\text{N/mm}^2$ . Determine the normal stress, shear stress and resultant stress on an oblique plane inclined at an angle of  $45^\circ$  with the axis of minor tensile stress.

### Given Data

Major principal stress,  $\sigma_1 = 80\text{N/mm}^2$

Minor principal stress,  $\sigma_2 = 40\text{N/mm}^2$

Shear stress  $r = 60\text{N/mm}^2$

Angle of oblique plane with the axis

of minor principal stress,  $\theta = 45^\circ$

### To find

The normal, tangential and resultant stresses.

### Solution.

#### Normal stress( $\sigma_n$ )

$$\begin{aligned}
 &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\theta + r \sin 2\theta \\
 &= \frac{80 + 40}{2} + \frac{80 - 40}{2} \cos(2 \times 45) + 60 \times \sin 2 \times 45 \\
 &= 120\text{N/mm}^2
 \end{aligned}$$

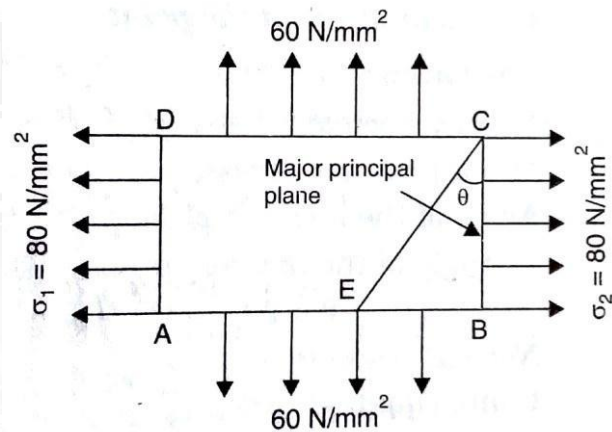
#### Tangential stress( $\sigma_t$ )

$$\begin{aligned}
 \sigma_t &= \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta - r \cos 2\theta \\
 &= \frac{80 - 40}{2} \sin(2 \times 45) - 60 \times \cos(2 \times 45) \\
 &= 20\text{N/mm}^2.
 \end{aligned}$$

#### Resultant stress( $\sigma_R$ )

The resultant stress on the section FC will be given as

$$\begin{aligned}
 \sigma_R &= \sqrt{\sigma_n^2 + \sigma_t^2} \\
 &= \sqrt{120^2 + 20^2} = 121.655\text{N/mm}^2
 \end{aligned}$$



**Problem 1.5.6.** A rectangular block of material is subjected to a tensile stress of  $110\text{N/mm}^2$  on one plane and a tensile stress of  $47\text{N/mm}^2$  on the plane right angles on the former. Each of the above stresses is accompanied by a shear stress of  $63\text{N/mm}^2$  and that associated with the former tensile stress tends to rotate the block anticlockwise. Find (i) the direction and magnitude of each of the principal stress and (ii) magnitude of the greatest shear stress.

### Given Data

Major principal stress,  $\sigma_1 = 110\text{N/mm}^2$

Minor principal stress,  $\sigma_2 = 47\text{N/mm}^2$

Shear stress  $r = 63\text{N/mm}^2$

### To find

- The direction and magnitude of each of the principal stress and
- The magnitude of the greatest shear stress.

### Solution

#### (i) Direction and Magnitude of principal stresses.

#### Major Principal stress

$$\begin{aligned} &= \frac{\sigma_1 + \sigma_2}{2} + \sqrt{\left(\frac{\sigma_1 - \sigma_2}{2}\right)^2 + r^2} \\ &= \frac{110 + 47}{2} + \sqrt{\left(\frac{110 - 47}{2}\right)^2 + 63^2} \\ &= 148.936\text{N/mm}^2. \end{aligned}$$

#### Minor Principal stress

$$\begin{aligned} &= \frac{\sigma_1 + \sigma_2}{2} - \sqrt{\left(\frac{\sigma_1 - \sigma_2}{2}\right)^2 + r^2} \\ &= \frac{110 + 47}{2} - \sqrt{\left(\frac{110 - 47}{2}\right)^2 + 63^2} = 8.064\text{N/mm}^2 \end{aligned}$$

#### Direction of Resultant stress

$$\tan 2\theta = \frac{2c}{\sigma_1 - \sigma_2} = \frac{2 \times 63}{110 - 47} = 2$$

$$2\theta = \tan^{-1} 2 = 63^\circ 26' \text{ or } 243^\circ 26'$$

$$\text{Or } \theta = 31^\circ 43' \text{ or } 121^\circ 26'$$

#### (ii) Magnitude of greatest shear stress

$$\begin{aligned} (\sigma)_{\text{max}} &= \frac{1}{2} \sqrt{(\sigma_1 - \sigma_2)^2 + 4r^2} \\ &= \frac{1}{2} \sqrt{(110 - 47)^2 + 4 \times 63^2} = 70.436\text{N/mm}^2 \end{aligned}$$

