# ROHINI COLLEGE OF ENGINEERING AND TECHNOLOGY DEPARTMENT OF MECHANICAL ENGINEERING



## ME3391 ENGINEERING THERMODYNAMICS

UNIT III ENTROPY

## Entropy

The second law leads to the definition of a new property called *entropy*.

## **The Clausius Inequality**

The first law is simply an energy balance. However, the second law leads to an inequality; an *irreversible* process is less efficient than a reversible process. Another important inequality in thermodynamics is the *Clausius* inequality:

$$\oint \frac{\delta Q}{T} \le 0$$

That is, the cyclic integral of  $\delta Q / T$  is always less than or equal to zero. This is valid for all cycles, reversible or irreversible.

For internally reversible cycles, it can be shown that:

$$\oint \frac{\delta Q}{T} \bigg|_{\text{int,rev}} = 0$$

## Entropy

The Clausius inequality forms the basis for the definition of a new property called entropy. As can be seen in the equation above, for an internally reversible process the cyclic integral of  $\delta Q / T$  is zero. A quantity whose cyclic integral is zero depends on the *state* only and not the process path, and thus it is a *property*.

Clausius in 1865 realized that he discovered a new property and he called it *entropy*:

$$dS = \left(\frac{\delta Q}{T}\right)_{\text{int,}rev} \qquad (\text{kJ/K})$$

Entropy per unit mass is designated by *s* (kJ/kg.K).

The entropy change of a system during a process can be calculated:

$$\Delta S = S_2 - S_1 = \int_{1}^{2} \left( \frac{\delta Q}{T} \right)_{\text{int,rev}} \qquad (\text{kJ/K})$$

To perform this integral, one needs to know the relation between Q and T during the process.

Note that the cyclic integral of  $\delta Q / T$  will give us the entropy change *only if* the integration carried out along an internally reversible path between two states.

For irreversible processes, we may imagine a reversible process between the two states (initial and final) and calculate the entropy change (since entropy is a property).

### The Increase of Entropy Principle

Entropy change of a closed system during an irreversible process is greater that the integral of  $\delta Q$  / T evaluated for the process. In the limiting case of a reversible process, they become equal.

$$dS \ge \frac{\delta Q}{T}$$

The entropy generated during a process is called *entropy generation*, and is denoted by  $S_{gen}$ ,

$$\Delta S = S_2 - S_1 = \int_1^2 \frac{\delta Q}{T} + S_{gen}$$

Note that the entropy generation S<sub>gen</sub> is *always a positive quantity or zero* (reversible process). Its value depends on the process, thus it **is not a property** of a system.

The entropy of an isolated system during a process always increases, or in the limiting case of a reversible process remains constant (it never decreases). This is known as the increase of entropy principle.

The entropy change of a system or its surroundings can be negative; but entropy generation cannot.

$\left  > 0 \right $	irreversible process
$S_{gen} = \begin{cases} = 0 \end{cases}$	reversible process
< 0	impossible process

1- A process must proceeds in the direction that complies with the increase of entropy principle,  $S_{gen} > 0$ . A process that violates this principle is impossible.

2- Entropy is a non-conserved property, and there is no such thing as the conservation of entropy. Therefore, the entropy of universe is continuously increasing.

3- The performance of engineering systems is degraded by the presence of irreversibility. The entropy generation is a measure of the magnitudes of the irreversibility present during the process.

## **Entropy Balance**

Entropy is a measure of molecular disorder or randomness of a system, and the second law states that entropy can be created but it cannot be destroyed.

The increase of entropy principle is expressed as

Entropy change = Entropy transfer + Entropy generation

$$\Delta S_{system} = S_{transfer} + S_{gen}$$

This is called the entropy balance.

## **Entropy Change**

The entropy balance is easier to apply that energy balance, since unlike energy (which has many forms such as heat and work) entropy has only one form. The entropy change for a system during a process is:

Entropy change = Entropy at final state - Entropy at initial state

$$\Delta S_{system} = S_{final} - S_{initial}$$

Therefore, the entropy change of a system is zero if the state of the system does not change during the process. For example *entropy change of steady flow devices* such as nozzles, compressors, turbines, pumps, and heat exchangers is *zero during steady operation*.

## Mechanisms of Entropy Transfer

Entropy can be transferred to or from a system in two forms: heat transfer and mass flow. Thus, the entropy transfer for an adiabatic closed system is zero.

<u>Heat Transfer</u>: heat is a form of disorganized energy and some disorganization (entropy) will flow with heat. Heat rejection is the only way that the entropy of a fixed mass can be decreased. The ratio of the heat transfer Q/ T (absolute temperature) at a location is called entropy flow or entropy transfer

Entropy transfer with heat (T = const.) 
$$S_{heat} = \frac{Q}{T}$$

Since T (in Kelvin) is always positive, the direction of entropy transfer is the same of the direction of heat transfer.

When two systems are in contact, the entropy transfer from warmer system is equal to the entropy transfer to the colder system since the boundary has no thickness and occupies no volume.

Note that **work is entropy-free**, and no entropy is transferred with work.

<u>Mass Flow</u>: mass contains entropy as well as energy, both entropy and energy contents of a system are proportional to the mass. When a mass in the amount of *m* enters or leaves a system, entropy in the amount of *ms* (*s* is the specific entropy) accompanies it.

## **Entropy Balance for a Closed System**

A closed system includes no mass flow across its boundaries, and the entropy change is simply the difference between the initial and final entropies of the system.

The entropy change of a closed system is due to the entropy transfer accompanying heat transfer and the entropy generation within the system boundaries:

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Entropy change of the system = Entropy transfer with heat + Entropy generation
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$$S_2 - S_1 = \sum \frac{Q_k}{T_k} + S_{gen}$$

Therefore, for an adiabatic closed system, we have:

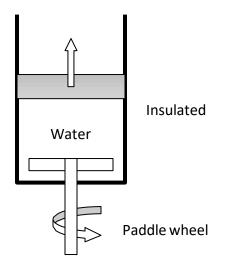
$$\Delta S_{adiabatic} = S_{gen}$$

For an internally reversible adiabatic process  $\Delta S = 0$ , because  $S_{gen} = 0$ .

The total entropy generated during a process can be determined by applying the entropy balance to an extended system that includes both the system and its immediate surroundings where external irreversibility might be occurring.

#### Example 1: Entropy balance for a closed system

Saturated liquid water at 100 C is contained in a piston-cylinder assembly. The water undergoes a process to the corresponding saturated vapor state, during which the piston moves freely in the cylinder. There is no heat transfer with the surroundings. If the change of state is brought about by the action of a paddle wheel, determine the network per unit mass, in kJ/kg, and the amount of entropy produced per unit mass, in kJ/kg.K.



Assumptions:

1- The water in the piston-cylinder assembly is a closed system.

2- There is no heat transfer with the surroundings.

3- The system is at an equilibrium state initially and finally.  $\Delta PE = \Delta KE = 0$ .

#### Solution

The network can be calculated by using the law:

$$\Delta U + \Delta KE + \Delta PE = Q - W$$

That is simplifies to:  $\Delta U = -W$ 

On a unit mass basis, the energy balance becomes:

$$W / m = - (u_g - u_f)$$

From Table A-4,

The negative sign indicates that the work input by the stirring is greater than the work done by the water as it expands.

Using an entropy balance, the amount of entropy produced can be found. Since there is no heat transfer,

$$\Delta S = \int_{0}^{2} \left( \frac{\delta Q}{T} \right) + S_{gen} = S_{gen}$$

On a unit mass basis, this becomes:

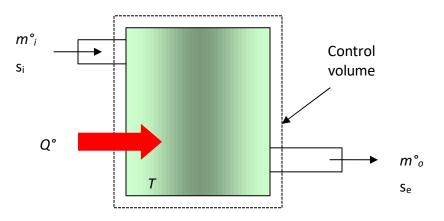
$$S_{gen}/m = s_g - s_f$$

Using Table A-4

$$S_{gen} / m = 6.048 \text{ kJ} / \text{kg.K}$$

#### **Entropy Balance for a Control Volume**

In addition to methods discussed for closed system, the entropy can be exchanged through *mass flows* across the boundaries of the control volume.



The entropy balance in the rate form for a control volume becomes:

$$\frac{dS}{\frac{CV}{dt}} = \sum \frac{Q^{\bullet}}{\frac{k}{T_k}} + \sum m_i^{\bullet} s_i^{\bullet} - \sum m_{e^{\bullet}e}^{\bullet} + S_{gen,CV}^{\bullet}$$

For a steady-state steady-flow process, it simplifies to:

$$S_{gen,CV}^{\bullet} = \sum m_e^{\bullet} s_e - \sum m_i^{\bullet} s_i - \sum_{k=1}^{Q} \frac{\Phi}{T_k}$$

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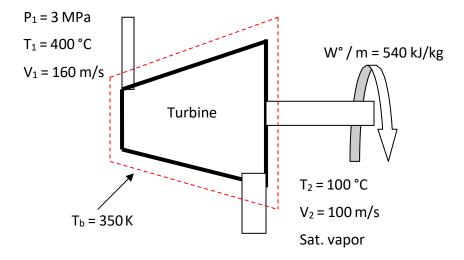
#### Example 2: Entropy balance for a CV

Steam enters a turbine with a pressure of 3 MPa, a temperature of 400 °C, and a velocity of 160 m/s. Saturated vapor at 100 °C exits with a velocity of 100 m/s. At steady-state, the turbine develops work equal to 540 kJ/kg. Heat transfer between the turbine and its surroundings occur at an average outer surface temperature of 350 K. Determine the rate at which entropy is produced within the turbine per kg of steam flowing, in kJ/kg.K. Neglect the change in potential energy between inlet and exit.

Assumptions:

1-Steady state operation in CV.  $\Delta PE = 0$ .

2-Turbine outer surface is at a specified average temperature.



From the mass balance, we know that  $m^\circ = m_1^\circ = m_2^\circ$ 

Since the process is steady-state, one can write:

$$0 = \sum_{\underline{x}} \frac{Q}{\underline{x}} \cdot m^{\bullet}(sT_{k\,i} - s_e) + S^{\bullet}_{gen,CV}$$

The heat transfer occurs at  $T_b$  = 350 K, the first term of the right hand side of the entropy balance reduces to  $Q^{\circ}/T_b$ 

$$\frac{S_{gen,CV}}{m^{\bullet}} = -\frac{Q_k}{m^{\bullet}T_k} + (s_2 - s_1)$$

We need to calculate the rate of heat transfer. The first law (energy balance) can be used to find the heat transfer rate. Combining the mass balance and the first law, one finds:

$$\frac{Q_{CV}^{\bullet}}{m^{\bullet}} = \frac{W_{CV}^{\bullet}}{m^{\bullet}} + (h_2^{-}h_1^{-}) + \left(\frac{V_2^2 - V_1^2}{2}\right)$$

From Table A-6,  $h_1$  = 3230.9 kJ/kg, and From A-4  $h_2$  = 2676.1 kJ/kg. After substitution, and converting the units, one finds:

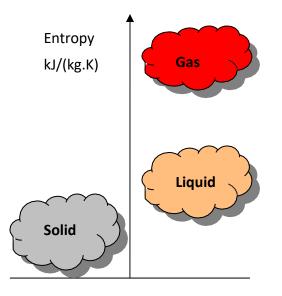
$$\frac{Q_{CV}^{\bullet}}{m^{\bullet}} = -22.6 \quad kJ / kg$$

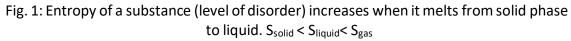
From Table A-4,  $s_2 = 7.3549 \text{ kJ/kg.K}$  and from Table A-6,  $s_1 = 6.9212 \text{ kJ/kg.K}$ . Inserting values into the expression for entropy production:

$$\frac{S_{gen,CV}^{\bullet}}{m^{\bullet}} = -\frac{Q_k^{\bullet}}{m^{\bullet}T_k} + (s_2 - s_1) = 0.4983 \quad kJ / kg.K$$

#### Entropy

Entropy can be viewed as a measure of molecular disorder, or molecular randomness. As a system becomes more disordered, the positions of the molecules become less predictable and the entropy increases.





#### Some remarks:

Work is an organized form of energy, free of disorder or randomness, thus free of entropy. Therefore, there is *no entropy associated with energy transfer as work*.

The *quantity* of energy is always preserved during an actual process, based on the *first law*, but the *quality* is bound to decrease (*the second law*).

Processes can occur only in the direction of *increased overall entropy* or molecular disorder. Thus, the entire universe is getting more and more chaotic every day.

At *absolute zero* (0 K), molecules become completely motionless, this represents a state of ultimate molecular order (and *minimum energy*). Therefore, the entropy of a pure

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crystalline substance at zero temperature is zero. That is because; there is *no uncertainty* about the state of the molecules at that instant. This statement is the **third law of thermodynamics**.

Since there is a reference for entropy (absolute zero), entropy is an absolute property. The entropy measured with respect to absolute zero is called absolute entropy.

The two diagrams used most extensively in the second-law analysis are the T-s and h-s diagrams. For an internally reversible process, one can write:

$$\delta Q_{\text{int,rev}} = T ds$$
 (kJ)

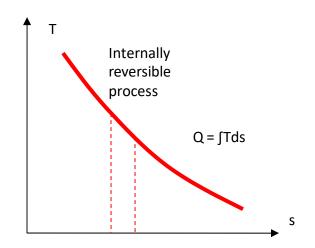


Fig. 2: On a T-s diagram, the area under an internally reversible process presents the heat transfer for the process.

For an internally reversible isothermal process, we have:

$$Q_{\text{int,rev}} = T_0 \, ds$$

In a T-s diagram, an isentropic process is represented by a vertical line. An isentropic process is a process in which entropy remains constant. As a result an isentropic process involves no heat transfer. Therefore:

Isentropic process  $(s_2 = s_1) = \text{Reversible} + \text{Adiabatic}$ 

## **Evaluation of Entropy Change**

The differential form of the conservation of energy for a closed system (fixed mass) for an internally reversible process is:

$$\delta Q_{int,rev} - \delta W_{int,rev} = dU$$

where,

$$\delta Q_{int,rev} = TdS$$
  
 $\delta W_{int,rev} = PdV$ 

Thus,

$$TdS = dU + PdV$$

or, per unit mass

Tds = du + Pdv

This is called the *first Gibbs equation*.

From the definition of enthalpy, h = u + Pv, one can find:

$$h = u + Pv \rightarrow dh = du + Pdv + vdP$$

Eliminating du from the first Gibbs equation, one finds the second Gibbs equation:

$$Tds = dh - vdP$$

Explicit relations for differential changes in entropy can be obtained from Gibbs equations:

$$ds = \frac{du}{T} + \frac{Pdv}{T}$$
$$ds = \frac{dh}{T} - \frac{vdP}{T}$$

To calculate the entropy change, we must know the relationship between du or dh and temperature.

### **Calculation of the Entropy for Saturated Mixture**

Use Tables A-4 and A-5 to find  $s_f$ ,  $s_g$  and/or  $s_{fg}$  for the following:

$$s = (1 - x)s_f + x s_g$$
 or  $s = s_f + x s_{fg}$ 

## **Calculation of the Entropy for Superheated Vapor**

Given two properties or the state, such as temperature and pressure, use Table A-6.

## Calculation of the Entropy for Compressed Liquid

In the absence of compressed liquid data for a property  $s \approx s_{f@T}$ 

## **Entropy Change of Solids and Liquids**

Solids and liquids can be assumed as incompressible substances since their volumes remains essentially constant during a process. Thus, the first Gibbs equation becomes:

$$ds = \frac{du}{T} = \frac{cdT}{2}$$
$$dT$$
$$s_2 - s_1 = \int c(T) \ T$$

Assuming an averaged value for specific heat, one obtains:

$$s_2 - s_1 = c_{ave} \ln \frac{T_2}{T_1}$$

Note that the entropy change of an incompressible substance is only a function of temperature. Therefore, for an *isentropic process* where  $s_2 = s_1$ , one can find:

$$T_2 = T_1$$

#### **Entropy Change of Ideal Gas**

The entropy change of an ideal gas can be obtained, by substituting  $du = c_v dT$  and P = RT/v into Gibbs equation.

$$ds = c_v \frac{dT}{T_2} + R \frac{dv}{v}$$
$$s_2 - s_1 = \int_1^1 c_v(T) \frac{dT}{T} + R \ln \frac{v}{v_1}$$

Assuming averaged values for specific heats, one obtains:

$$s_{2} - s_{1} = c_{v,ave} \ln \frac{T_{2}}{T_{1}} + R \ln \frac{v_{2}}{v_{1}} \qquad \frac{kJ}{kg.K}$$

$$s_{2} - s_{1} = c_{p,ave} \ln \frac{T_{2}}{T_{1}} - R \ln \frac{P_{2}}{P_{1}} \qquad \frac{kJ}{kg.K}$$

For isentropic processes of ideal gases, the following relationships can be found by setting ds = 0,

$$\ln \frac{T_2}{T_1} = -\frac{R}{C_v} \ln \frac{v_2}{v_1}$$

Since  $R = c_p - c_v$ ,  $k = c_p / c_v$ , and thus  $R / c_v = k - 1$ .

In a similar manner, one finds:

$$\begin{pmatrix} T_{2} \\ T_{1} \end{pmatrix} = \begin{pmatrix} P_{2} \\ P_{1} \end{pmatrix}^{(k-1)/k} \text{ isentropic process}$$
$$\begin{pmatrix} P_{2} \\ P_{1} \end{pmatrix} = \begin{pmatrix} v_{1} \\ v_{2} \end{pmatrix}^{k} \text{ isentropic process}$$

These equations can be expressed in the following compact forms:

$$Tv^{k-1} = \text{constant}$$

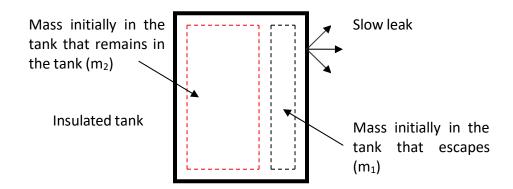
$$TP^{(1-k)/k} = \text{constant}$$

#### $Pv^k$ = constant

The specific ratio k, varies with temperature, and in isentropic relations above an average k value should be used.

#### Example 3: Isentropic process of ideal gas

A rigid, well-insulated tank is filled initially with 5 kg of air at pressure 500 kPa and a temperature 500 K. A leak develops, and air slowly escapes until the pressure of the air remaining in the tank is 100 kPa. Using the ideal gas model, determine the amount of mass remaining in the tank and its temperature.



Assumptions:

1- As shown in the figure, the closed system is the mass initially in the tank that remains in the tank.

2- There is no significant heat transfer between the system and its surroundings.

3- Irreversibilities within the tank can be ignored as the air slowly escapes.

Solutions:

Using the ideal gas equation of state, the mass initially in the tank that remains in the tank at the end of process is:

$$m_1 = \frac{P_2 V}{\frac{P_1 V}{RT_1}}$$

Since the volume of the tank V remains constant during the process. We need to find the final temperature  $T_2$ . For the closed system under consideration ( $m_1$ ), there are no irreversibilities, and no heat transfer. Accordingly, it is an *isentropic* process, and thus the isentropic relationships can be used:

$$\frac{T}{\frac{2}{T_{1}}} = \left(\frac{P}{\frac{2}{P_{1}}}\right)^{(k-1)/k} \qquad T_{2} = T_{1} \left(\frac{P_{2}}{P_{1}}\right)^{(k-1)/k}$$

With a constant *k* = 1.4 for air, after substituting values, one finds:

Finally, inserting values into the expression for system mass

#### **Reversible Steady-Flow Work**

The conservation of energy equation for a steady-flow device undergoing an internally reversible process can be expressed in differential form as

$$\delta q_{rev} - \delta w_{rev} = dh + dke + dpe$$
But
$$\delta q_{rev} = Tds$$

$$\rightarrow \delta q = dh - vdP$$

$$Tds = dh - vdP$$

Substituting into the relation above, after canceling dh, it yields,

$$-\delta w_{rev} = vdP + dke + dpe$$

Integrating, we find

$$w_{rev} = -\int_{1}^{2} v dP - \Delta ke - \Delta pe \qquad (kJ / kg)$$

With negligible changes in potential and kinetic energies,

$$w_{rev} = -\int_{1}^{2} v dP \qquad (kJ / kg)$$

From the above equation can be seen that, the larger the specific volume the larger the reversible produced or consumed work by the steady-flow device. Thus, every effort should be made to keep the specific volume of the flow as small as possible during a compression process to minimize the input work.

When the fluid is incompressible, the specific volume remains constant during the process, thus the above equation becomes:

$$\delta w_{rev} = v(P_1 - P_2) - \Delta ke - \Delta pe$$
 (kJ/kg)

For a steady-state flow of a liquid through a device that involves no work interactions (such as nozzle or a pipe section), the work term is zero,

$$v(P_2 - P_1) + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1) = 0$$

This is known as *Bernoulli equation* in fluid mechanics.