## UNDERGROUND RECTANGULAR TANKS - HEMISPHERICAL BOTTOMED STEEL WATER TANK

3.3 Design the closed rectangular water tank

## Example 3

Design the closed rectangular water tank with internal dimension of $6 \times 3 x$ 3 m below the ground level. The nature of soil is always dry and its unit weight $18 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ and angle of repose $28^{\circ}$. Draw the reinforcement detail.

Given data:

| Internal dimension | $=6 \times 3 \times 3 \mathrm{~m}$ |
| :--- | :--- |
| unit weight | $=18 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ |
| angle of repose | $=28^{\circ}$ |
| nature of soil | $=$ dry |

## Solution:

Step 1: Design of constants

The tank with the dimension of $6 \times 3 \times 3 \mathrm{~m}$ and 200 mm free board

$$
\begin{aligned}
6 \times 3 \times 2.8 & =50.4 \mathrm{~m}^{\wedge} 3 \\
& =50400 \text { liters capacity }
\end{aligned}
$$

Let useM20 grade concrete anf Fe 415 steel
permissible direct tensile stress of concrete,

$$
\sigma_{\mathrm{ct}}=1.2 \mathrm{Mpa}
$$

permissible bending tensile stress of concrete,

$$
\sigma_{\mathrm{cbt}}=1.6 \mathrm{Mpa}
$$

permissible bending compressive stress of concrete,

$$
\sigma_{\mathrm{cbc}}=7.0 \mathrm{Mpa}
$$

modular ratio,

$$
\begin{aligned}
\mathrm{m} & =280 / 3 \\
\sigma_{\mathrm{cbc}} & =280 / 3(7)
\end{aligned}
$$

$$
=13.33
$$

permissible tensile stress of steel ${ }_{\sigma s t}=150 \mathrm{MPa}$
N.A depth coefficient, $\quad \mathrm{n}=1 / 1+\sigma_{\mathrm{st}} / \mathrm{m} \sigma_{\mathrm{cbc}}$

Lever arm coefficient

$$
\begin{aligned}
\mathrm{j} & =1-\mathrm{n} / 3 \\
& =0.872 \\
\mathrm{~K} & =1 / 2 \sigma_{\mathrm{cbc}} \mathrm{nj} \\
& =1 / 2 \times 7 \times 0.3835 \times 0.872 \\
& =1.170
\end{aligned}
$$

Step 2:Design of walls
(i) Testing condition (tank full of water without support of surrounding soil)
(ii) Empty tank condition
(i) Only water pressure acting on the tank wall from inside.

Maximum water pressure, $\quad \mathrm{P} \quad=\gamma \mathrm{H}$

$$
\begin{aligned}
& =10 \times 3 \\
& =30 \mathrm{kN} / \mathrm{m}^{\wedge} 2
\end{aligned}
$$



Bending moment @ water face

$$
\begin{aligned}
\mathrm{PH}^{\wedge} 2 / 15 & =30 \times 3^{\wedge} 2 / 15 \\
& =18 \mathrm{kNm} / \mathrm{m}
\end{aligned}
$$

Bending moment @ away from water face

$$
\begin{aligned}
\mathrm{PH}^{\wedge} 2 / 33.5 & =30 \times 3^{\wedge} 2 / 33.5 \\
& =8.8 \mathrm{kNm} / \mathrm{m}
\end{aligned}
$$

Thickness of wall required for avoiding crack can be determined by,

$$
\begin{aligned}
\sigma_{\mathrm{cbt}} \times 1 / 6 \times b \times \mathrm{D}^{\wedge} 2 & =\mathrm{M} \\
1.6 \times 1 / 6 \times 1000 \times \mathrm{D}^{\wedge} 2 & =18 \times 10^{\wedge} 6 \\
\mathrm{D} & =260 \mathrm{~mm}
\end{aligned}
$$

Let provide 300m wall thickness.
(ii) Empty tank condition

Active earth pressure coefficient

$$
\begin{aligned}
\mathrm{K}_{\mathrm{a}} & =1-\sin \phi / 1+\sin \phi \\
& =1-\sin 28^{\circ} / 1+\sin 28^{\circ} \\
& =0.361
\end{aligned}
$$

Maximum earth pressure

$$
\begin{aligned}
\mathrm{P} & =\mathrm{K}_{\mathrm{a}} \gamma_{\mathrm{s}} \mathrm{H} \\
& =0.361 \times 18 \times 3 \\
& =19.5 \mathrm{kN} / \mathrm{m}^{\wedge} 2
\end{aligned}
$$

Bending moment @ base (away from water face)

$$
\mathrm{PH}^{\wedge} 2 / 15=19.5 \times 3^{\wedge} 2 / 15
$$

$$
=11.7 \mathrm{kNm} / \mathrm{m}
$$

## Calculating area of steel

Maximum bending moment @ water face

$$
=18 \mathrm{kNm}
$$

Maximum bending away from water face

$$
\begin{aligned}
& =11.7 \mathrm{kNm} \\
\text { Minimum required steel } & =0.24-300 / 350 \times 0.08 \\
& =0.17 \\
\mathrm{~A}_{\mathrm{st} \text { min }} & =0.17 / 100 \times 1000 \times 300 \\
& =510 \mathrm{~mm}^{\wedge} 2 \\
& =255 \mathrm{~mm}^{\wedge} 2 \text { on each face }
\end{aligned}
$$

Vertical reinforcement required @ water face

$$
\begin{aligned}
& =\mathrm{M} / \sigma_{\text {st }} \mathrm{jd} \\
& =18 \times 10^{\wedge} 6 / 150 \times 0.874 \times 250 \\
& =528 \mathrm{~mm}^{\wedge} 2
\end{aligned}
$$

Provide 12 mm @ $200 \mathrm{~mm} \mathrm{c} / \mathrm{c}$,( $\mathrm{A}_{\text {st pro }}=565 \mathrm{~mm}^{\wedge} 2$ ) vertical reinforcement on inner face of tank.

Vertical reinforcement away from water face

$$
\begin{aligned}
& =11.7 \times 10^{\wedge} 6 / 150 \times 0.874 \times 250 \\
& =343 \mathrm{~mm}^{\wedge} 2
\end{aligned}
$$

Provide $12 \mathrm{~mm} \Phi @ 300 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ spacing $\left(\mathrm{A}_{\text {st pro }}=377 \mathrm{~mm}^{\wedge} 2\right)$ on outer face of tank.
Provide 10 mm ф@ $200 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ as horizontal bars on the both face of wall.

Step 3 :Design of roof slab

Assume thickness of roof slab is 150 mm

Loading:

| (i) Self weight of slab | $=0.15 \times 24$ |
| ---: | :--- |
|  | $=3.8 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ |
| (ii) live load | $=1.5 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ |
| (iii) finishing | $=0.15 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ |
| c/c dimension of the slab | $=5.25 \mathrm{kN} / \mathrm{m}^{\wedge} 2$ |
| (ial | $=3.3 \times 6.3 \mathrm{~m}$ |

Design of oneway slab

The max bending moment in slab $=5.25 \times 3.3^{\wedge} 2 / 8$
$=7.146 \mathrm{kN}$
effective depth required $d=\sqrt{\frac{7.1465 \times 10^{6}}{1.012 \times 1000}}$
$\mathrm{d}_{\text {pro }}=150-40$
$=110 \mathrm{~mm}$
$=84 \mathrm{~mm}<110 \mathrm{~mm}$

Area of steel requirement

$$
\mathrm{A}_{\mathrm{st}} \quad=7.1465 \times 10^{\wedge} 6 / 150 \times 0.874 \times 110
$$

$$
=495.56 \mathrm{~mm}^{\wedge} 2
$$

Provide 12 mm ф@200 $\mathrm{mm} \mathrm{c} / \mathrm{c}$ along both directions.

Step 4: Design of base slab

The BM @ base of wall will be same for the edge of base slab.
Hence provide 300 mm thickness with 12 mm ф@ $200 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ at the top and 12mmф @
$300 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ at the bottom.

Reinforcement details


Fig.3.1 Cross section


Fig.3.2 Cross section

