

Plate Girders - Behavior Of Components

5.1 Design for plate girder with thick web

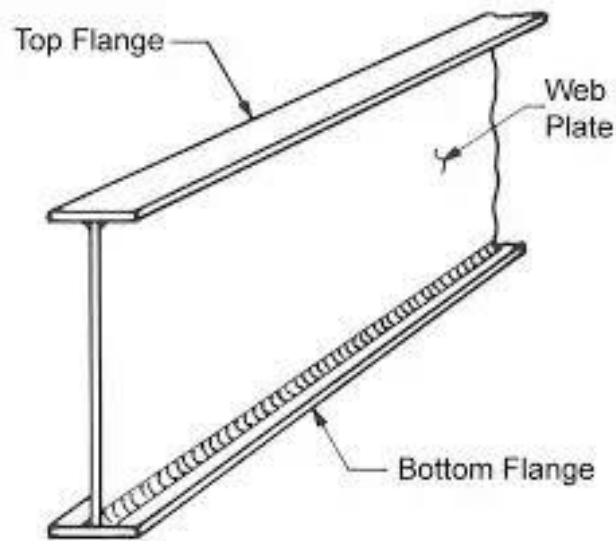


Fig 5.1 Plate girder

Design for plate girder with thick web

Example 1

Design a welded plate girder of 30m span to support a uniformly distributed load of 100kN/m over the span using the following data. Yield stress of steel is 250 N/mm², top flange restrained laterally. Design the cross sectional details of the plate girder to confirm to the specifications of IS 800-2007

Given data :

effective span of girder	= 30 m
Distributed live load	= 100kN/m
Yield stress of steel	= 250 N/mm ²

Step 1 : Load on plate girder

$$\begin{aligned}\text{load on girder} &= (1.5 \times 100 \times 30) \\ &= 4500\text{kN}\end{aligned}$$

$$\begin{aligned}\text{Assume self weight} &= (4500 / 200) \\ &= 22.5 \text{ KN/m}\end{aligned}$$

$$\begin{aligned}\text{Total factored load} &= 100 + 22.5 \\ &= 122.5 \text{ KN/m}\end{aligned}$$

Step 2 : Bending moments and shear force

$$\begin{aligned}M_d &= (WL^2 / 8) \\ &= (122.5 \times 30^2 / 8) \\ &= 13781 \text{ KNm}\end{aligned}$$

$$\begin{aligned}V_d &= (WL / 2) \\ &= (122.5 \times 30 / 2) \\ &= 1837.5 \text{ KN}\end{aligned}$$

Step 3 : Cross section of girder

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depth of plate girder

$$D = [(MK / f_y)]^{0.33}$$

$$K = (d / t_w) < 200 \text{ €}$$

$$d = \text{depth of web}$$

$$t_w = \text{thickness of web}$$

Yield stress ration

$$\text{€} = (250 / f_y)$$

$$= (250 / 250)$$

$$= 1$$

$$K = 200 \text{ €}$$

$$= 200 \times 1$$

$$= 200$$

$$D = [(13781 \times 10^6 \times 200 / 250)]^{0.33}$$

$$= 2060 \text{ mm}$$

$$\text{adopt overall depth } D = 2000 \text{ mm}$$

Allowing for 50mm flange plates

$$\text{Depth of web } d = 2000 - 100$$

$$= 1900 \text{ mm}$$

Thickness of web

$$(d / t_w) = 200 \text{ €}$$

$$T_w = d / 200 \times 1$$

$$= 1900 / 200$$

$$= 9.5 \text{ mm}$$

$$(d / t_w) = 67 \text{ €}$$

$$T_w = d / 67 \times 1$$

$$= 1900 / 67$$

$$= 28.3 \text{ mm}$$

adopt 25mm thick and 1900mm deep web

Width of flange

$$\text{Width of flange} = 0.2 d \text{ to } 0.3 d$$

$$= 0.2 \times 1900 \text{ to } 0.3 \times 1900$$

$$= 380 \text{ to } 570$$

$$= 450 \text{ mm}$$

adopt width of flange is 450mm

Check for plastic and compact section, the ratio

$$b / t_f < 9.4\epsilon$$

$$\epsilon = 1$$

$$t_f = 50\text{mm}$$

$$b_f = 450\text{mm}$$

$$450 / 50 = 9$$

The ratio satisfies the plastic section

Step 4 : Moment capacity

The moment capacity of the plate girder is

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$$M_d = [(\beta_b \times Z_p \times f_y) / \gamma_{mo}]$$

$$\beta_b = 1$$

$$Z_p = [(2 \times b_f \times t_f (D - t_f) / 2) + (t_w \times d^2) / 4]$$

$$= [(2 \times 450 \times 50 (2000 - 50) / 2) + (25 \times 1900^2) / 4]$$

$$= 66.43 \times 10^6 \text{ mm}^3$$

$$M_d = [(1 \times 66.43 \times 10^6 \times 250) / 1.1]$$

$$= 15097 \text{ KNm} > 13781 \text{ KNm}$$

Hence the section is safe

Step 5 : Shear capacity

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$$V < V_d$$

Design shear strength

$$V_d = V_n / \gamma_{mo}$$

$$V_n = V_p$$

$$V_p = [(A_v \times f_{yw}) / \sqrt{3}]$$

$$A_v = d \times t_w$$

$$= 1900 \times 25$$

$$= 47500 \text{ mm}^2$$

$$V_p = [(A_v \times f_{yw}) / \sqrt{3}]$$

$$= [(47500 \times 250) / \sqrt{3}]$$

$$= 68560.03 \times 10^3 \text{ N}$$

$$V_d = V_p / \gamma_{mo}$$

$$= 4099186 / 1.1$$

$$= 6232.75 \text{ KN} > 1837.5 \text{ KN}$$

Hence the section is safe

Step 6 : Check for bearing stiffeners

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$$F_w = (b_1 + n_2) t_w (f_y / \gamma_{mo})$$

Minimum stiffeners bearing length

$$b_1 = b_f / 2$$

$$= 450 / 2$$

$$= 225 \text{ mm}$$

$$n_2 = 2.5 \times 50$$

$$= 125 \text{ mm}$$

$$\begin{aligned}
 F_w &= (b_1 + n_2) t_w (f_y / \gamma_{mo}) \\
 &= (225 + 125) \times 25 \times (250 / 1.1) \\
 &= 1988.63 \times 10^3 \text{ KN} > 1837 \text{ KN}
 \end{aligned}$$

Hence safe

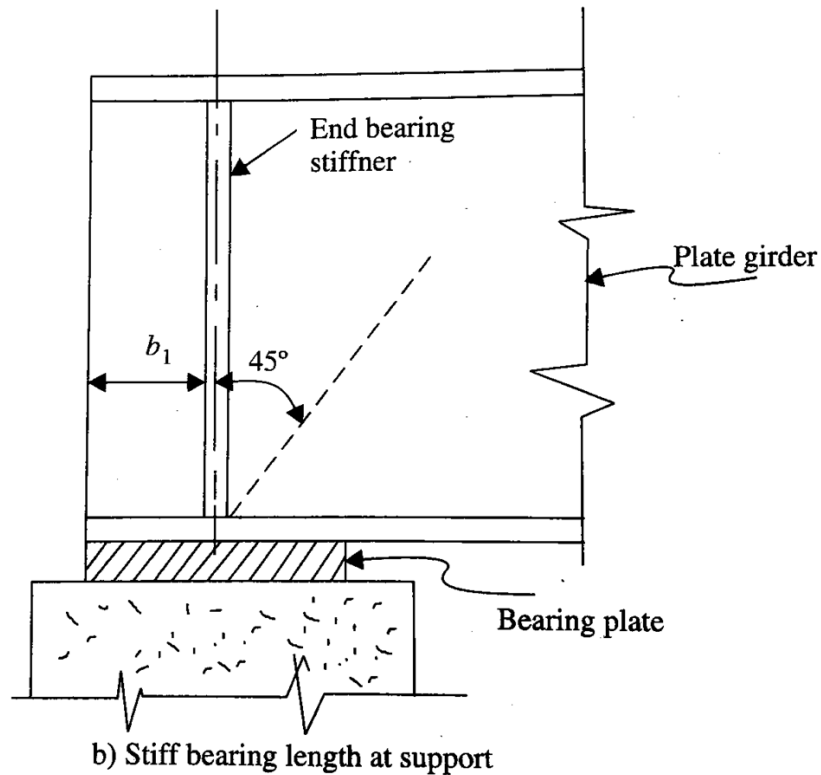


Fig.5.2 Stiff bearing